

## Reactive Loudspeaker Loads

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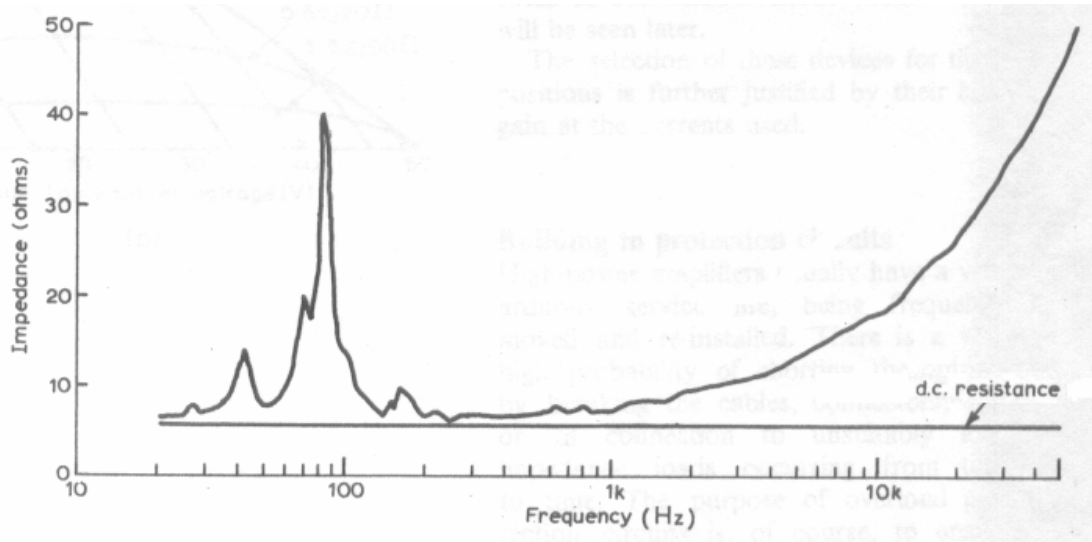
The impedance  $|Z\angle\theta^\circ|$  of any loudspeaker system may be assumed to consist of its *resistance*  $R$  (i.e. measured at DC) in series with an equivalent reactance  $X$  such that:

$$Z\angle\theta^\circ = (R \pm jX) \quad (1)$$

And

$$|Z\angle\theta^\circ| = \sqrt{(R^2 + X^2)} \quad (2)$$

The loudspeaker's resistance  $R$  (**fig. 1**) is *always* less than the magnitude of its impedance since  $|Z\angle\theta^\circ|_{(R>X)} > R$  and  $|Z\angle\theta^\circ|_{(X>R)} > X$ .



**Fig. 1. Impedance frequency response of a nominal 8Ω loudspeaker. The horizontal line represents its resistance of roughly 5Ω5. (After R. B. H. Becker, *Wireless World* February 1972, pg. 7).**

For instance at 1KHz a  $9.7\Omega\angle -55.5^\circ$  impedance consists of a 5Ω5 resistor in series with a 19μ9 capacitor; in this case the resistance alone is nearly half the magnitude of the total impedance at 1KHz.

If a loudspeaker system's input *resistance* (in contradistinction to its *nominal input impedance*) is known, then all possible combinations of its impedance are wholly described by  $Z\angle\theta^\circ = (R \pm j\infty)$ .

It is shown (**fig. 2**) that all possible characteristics described by  $Z\angle\theta^\circ = (R \pm j\infty)$  are bounded by a line (in red) of negative slope extending from the maximum current  $(V_{\text{Supply}}/R)$  demanded by the load to twice the magnitude  $(2|V_{\text{Supply}}|)$  of each supply rail.