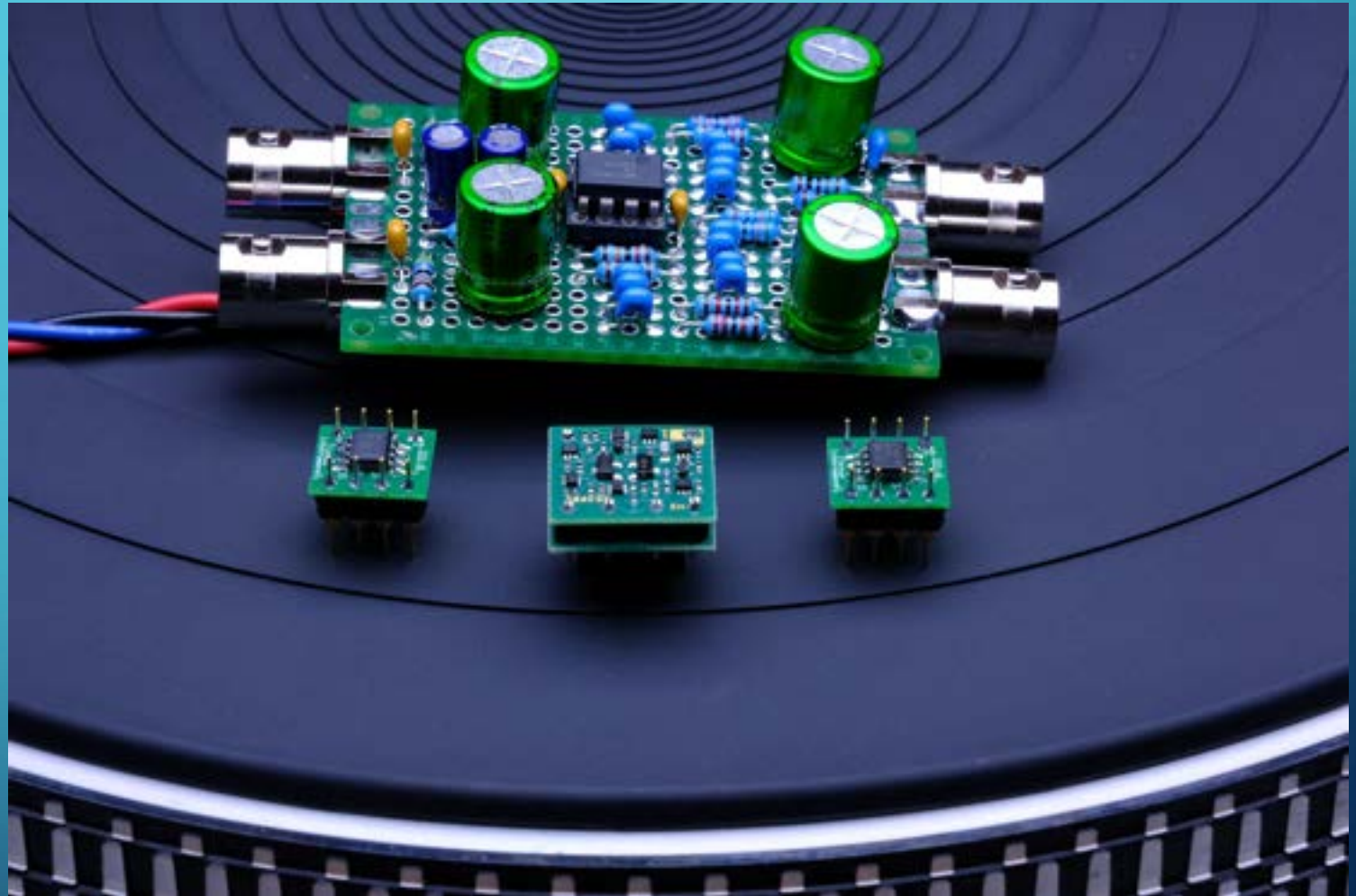


♪ ROLLING, ROLLING, ROLLING ♪



OPAMP ROLLING IN AUDIO APPLICATIONS
TOM CHRISTIANSEN

INTRODUCTION

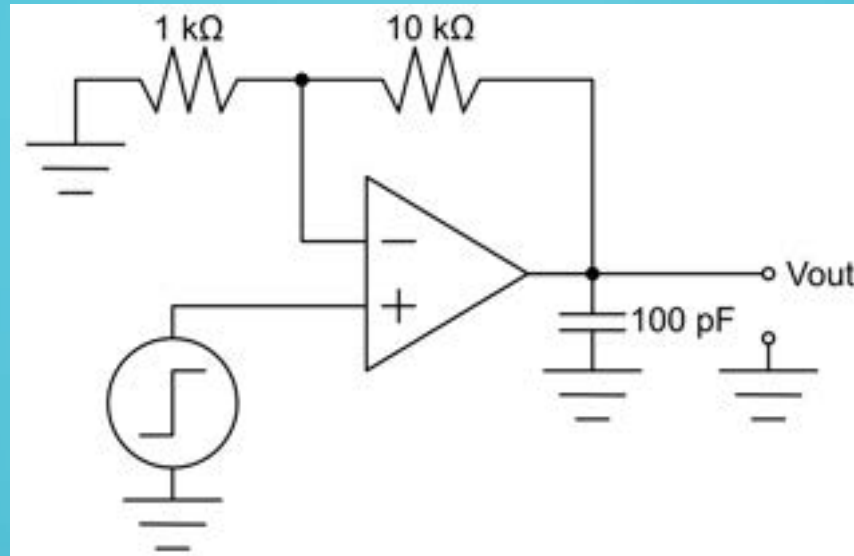
Tom Christiansen (tomchr)

- BScEE – Engineering College of Copenhagen – 1999
- MScEE – University of Washington, Seattle – 2002
- BA (Psych) – University of Calgary – 2019
- National Semiconductor – Federal Way, WA – 2005 - 2011
- Texas Instruments – Federal Way, WA – 2011 - 2015
- Neurochrome – Calgary, AB – 2010 - present

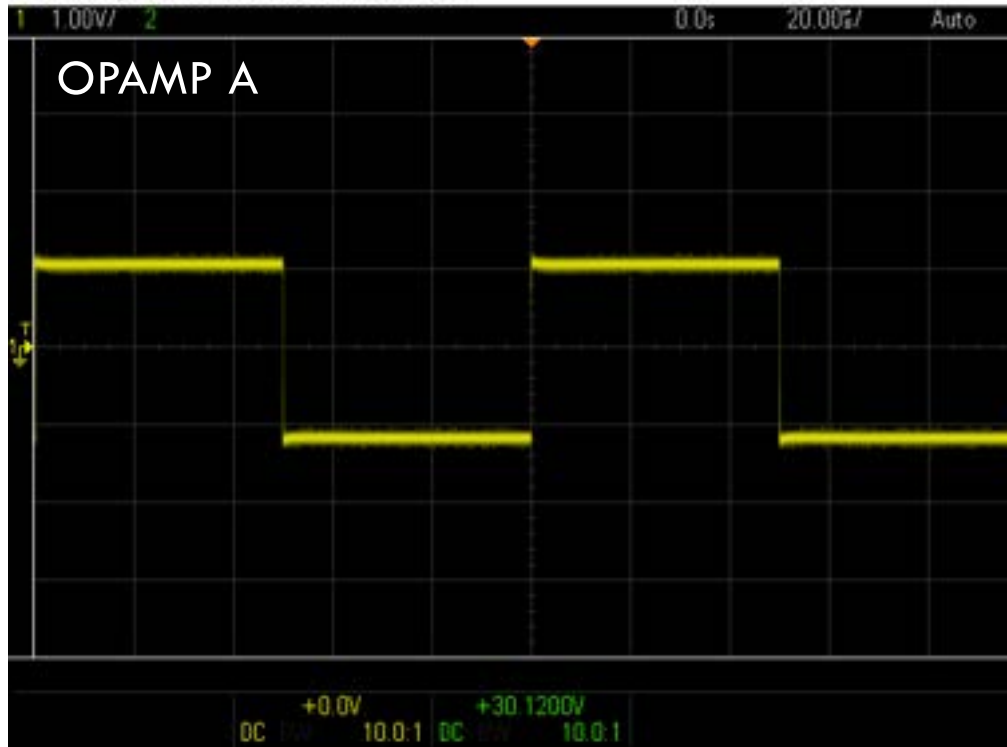


INTRODUCTION

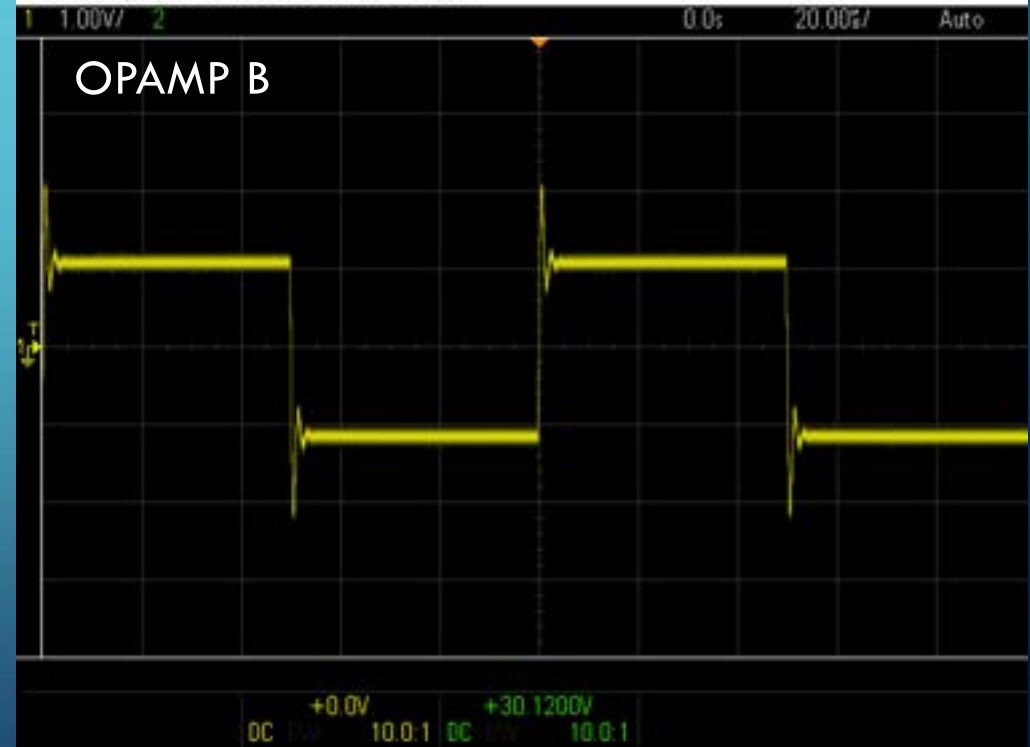




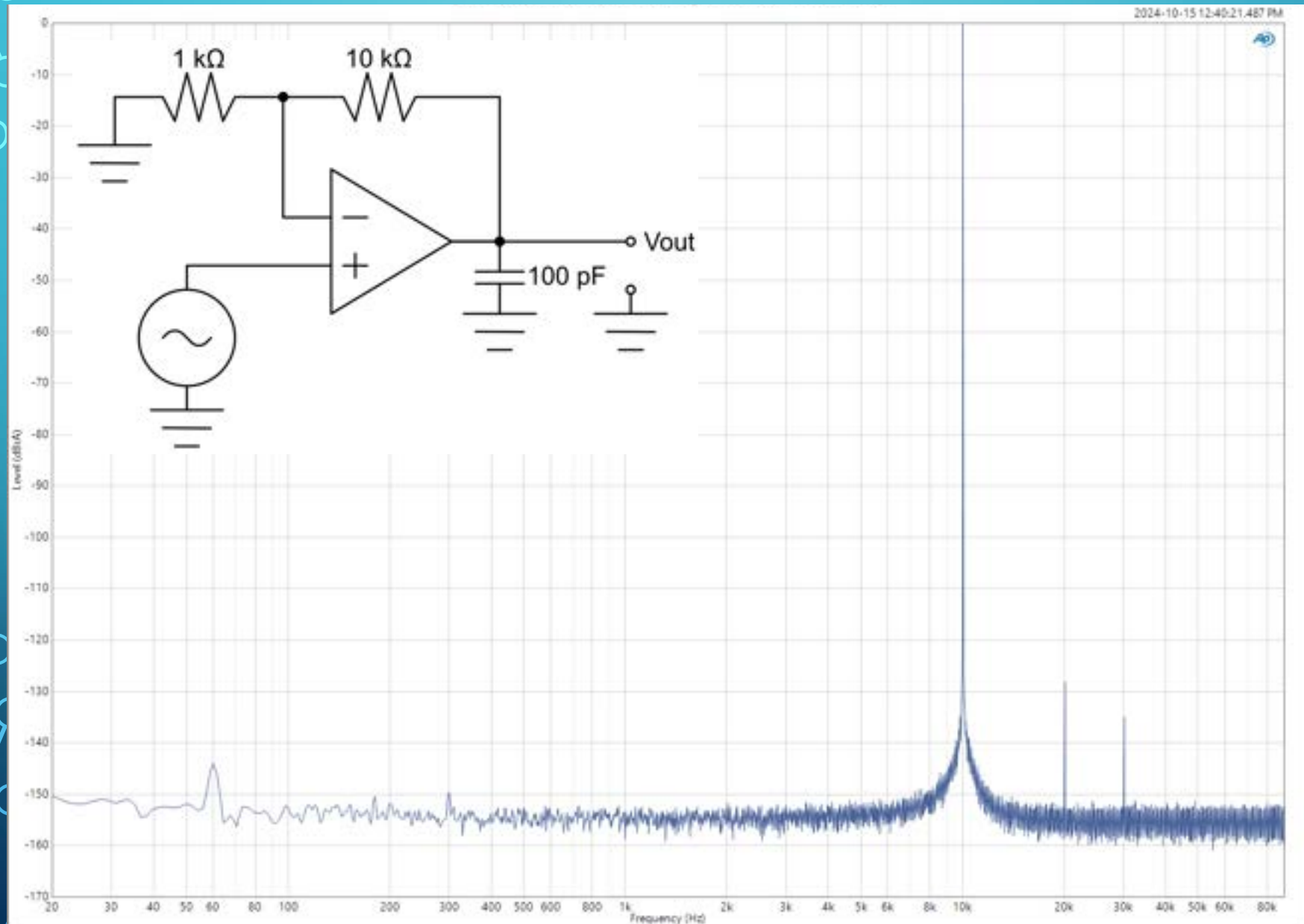
DSO-X 1102G, CN57496197: Sun Oct 13 15:37:37 2024



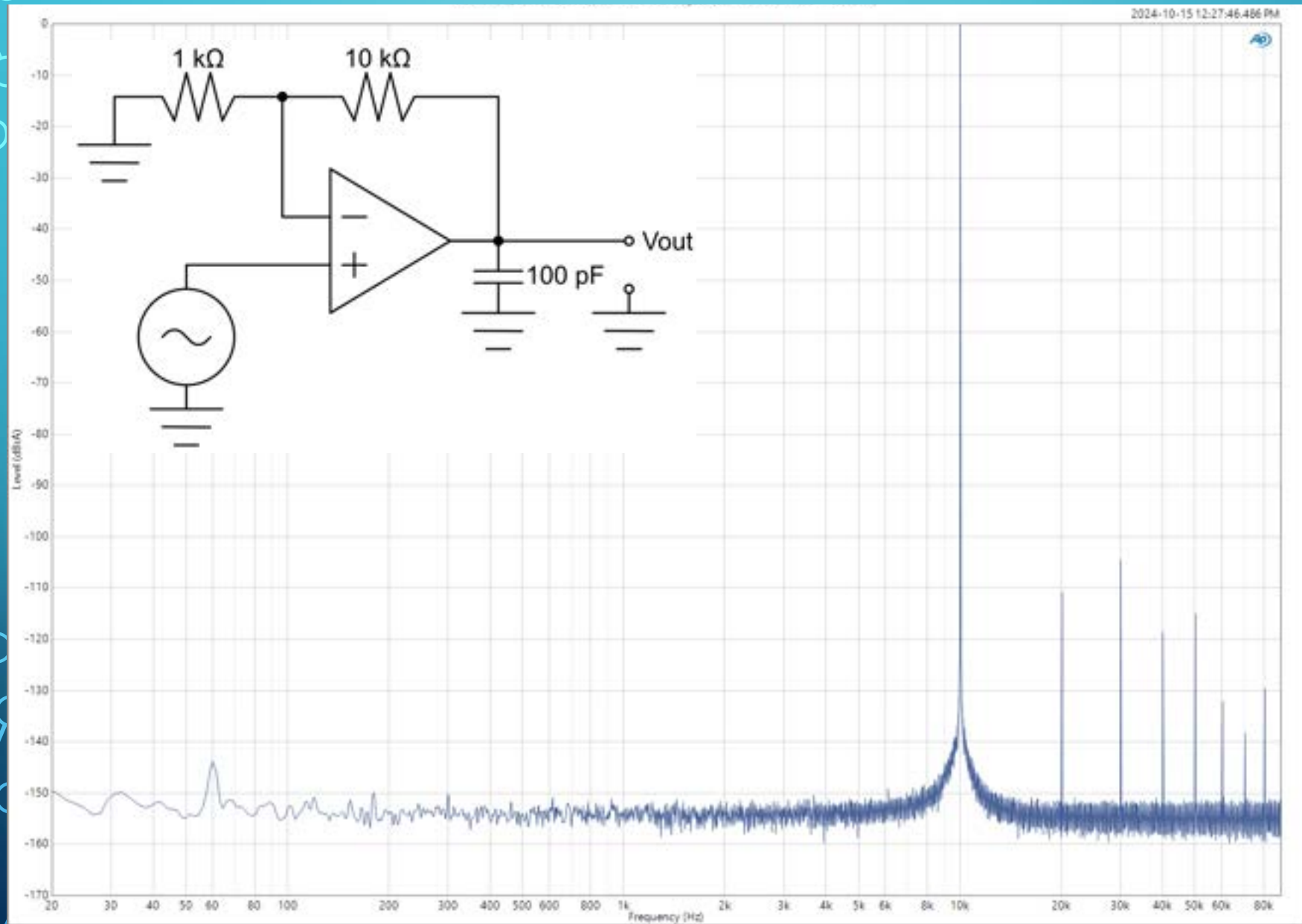
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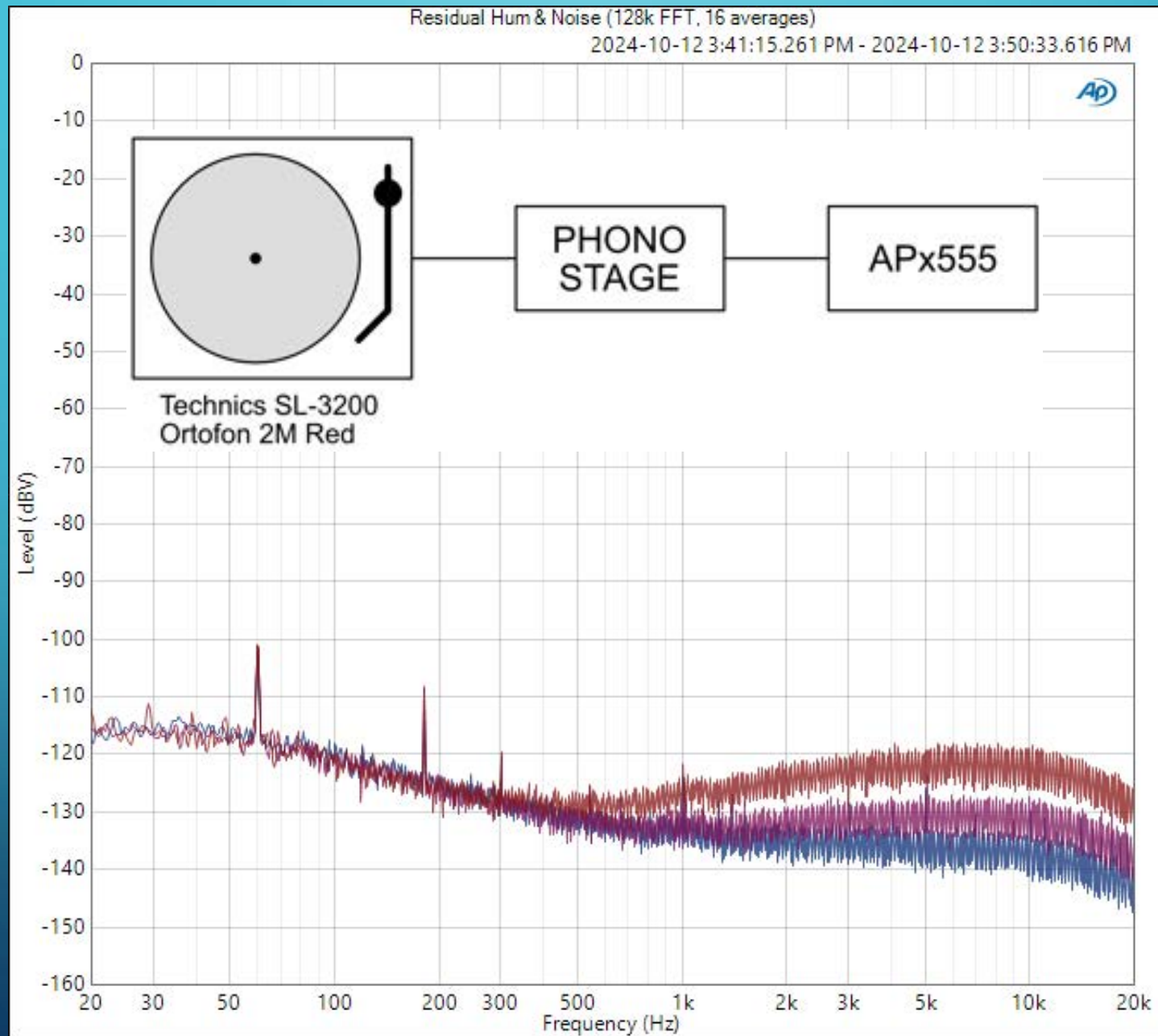


OPAMP A



OPAMP B

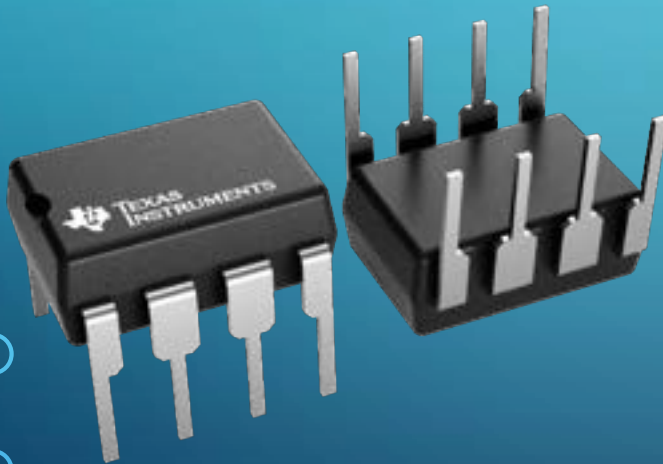




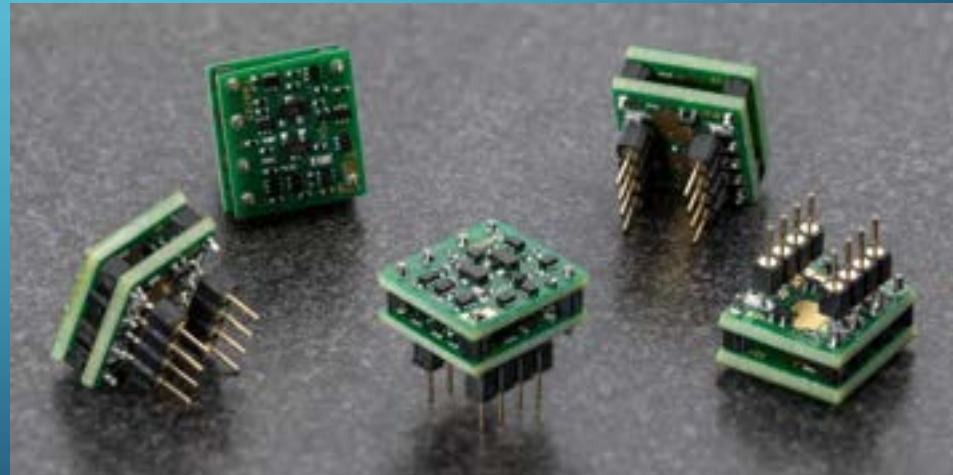
OPAMP A
OPAMP B
OPAMP C

OUR CONTESTANTS ARE ...

- OPAMP A \$6.59 TI OPA1612AIDR
- OPAMP B \$79.80 Sparkos SS3602 (Discrete)
- OPAMP C \$2.10 TI OPA1642AIDR



(Texas Instruments)



(Sparkos)

ROLL THE OPAMP – ROLL THE DICE

- Discrete vs Integrated
- Stability Analysis
- Real World Example #1 – Gain Stage
- Real World Example #2 – Phono Stage
- Lessons Learned
- Questions

DISCRETE VS INTEGRATED



Supreme Sound Opamp V7 Data

The Supreme Sound V7 Operational Amplifier (SS Opamp) is the product of a new development, leveraging a legacy of 20 years of expertise in audio technology. The operational amplifier is designed with a singular focus on delivering superior performance. In contrast to conventional integrated circuit operational amplifier designs, Burson's approach for the SS Opamp emphasises minimising open-loop drift, and achieving low offset. Furthermore, the SS Opamp distinguishes itself through its versatile power supply compatibility, key features for outstanding analog performance.

The design's input stage features a pair of meticulously matched field-effect transistors, followed by a two-stage screening process to ensure optimal compatibility and performance. This ensures consistent, high-quality amplification. The amplification core of the SS Opamp is moving away from traditional voltage amplification methods. This design approach, by reducing the current-limiting resistor's value, effectively reduces the RC parameter of the output stage, resulting in a faster response.

Enhancing its capabilities further, the SS Opamp includes another set of output transistors in the final stage, facilitating a high drive current and low output impedance. This makes the SS Opamp highly adaptable and suitable for various audio applications, providing robust performance and low output impedance.

Height: 20 mm
(0.78 inches)

Width: 15.4 mm
(0.60 inches)

Depth: 13.4 mm
(0.52 inches)

Dual: 5.7g (0.2 Ounce) Single: 4.5g (0.26 Ounce)

		Measurement		
Absolute Maximum Ratings		Min	Typ	Max
Supply Voltage		+/-4 V	+/-15V	+/- 16V
Operating Ambient Temperature		-25°C		60°C
Storage temperature range		-65°C		80°C
DC Characteristics		Testing Temperature 25°C Supply Voltage +/-15V		
Quiescent Current (mA)			Single 30mA Dual 20mA	
Input offset voltage (mV)	$I_k = 0$	0.05 mV	0.1 mV	
Input offset current (mA)		0.08 mA	0.12 mA	0.15 mA
Input BIAS current (μA)		120 μA	150 μA	300 μA
Common-Mode Rejection Ratio			100 dB	
Power Supply Rejection Ratio			15 μV/V	
AC Characteristics		Testing Temperature 25°C Supply Voltage +/-12V		
Open-loop gain (dB)			66 dB	
Open-loop bandwidth (dB)	$R_L = 600\Omega$		48 KHz	
Gain Bandwidth Product (MHz)	@ 100KHz		55 MHz	
Slew Rate (V/μs)	$f = 10\text{kHz}; R_S = 2K\Omega$		35V/μs	5V/μs
Input Resistance (kOhm)			50MΩ	
Crosstalk distortion (dB) [Dual Opamp]	$f = 1\text{kHz}; R_S = 600\Omega$		>96dB	
Total Harmonic Distortion (%) 1kHz @ 2V output	1kHz @ 2V output; $R_L = 600\Omega$		0.018%	
Output Impedance (Ohm)	$A_V = 30\text{dB}$ Closed-loop $f = 10\text{kHz}, R_L = 600\Omega$		0.40Ω	

(Burson)

DISCRETE VS INTEGRATED



OPA161x Sou

1 Features

- Superior Sound
- Ultralow Noise
- Ultralow Distortion
- High Slew Rate
- Wide Bandwidth
- High Open-Loop Gain
- Unity Gain Stable
- Low Quiescent Current
- Rail-to-Rail Output
- Wide Supply Range
- Single and Dual

2 Applications

- Professional Audio
- Microphone Preamp
- Analog and Digital
- Broadcast Studio
- Audio Test and Measurement
- High-End A/V Receivers

6.4 Electrical Characteristics: V

At $T_A = +25^\circ\text{C}$ and $R_L = 2\text{ k}\Omega$, unless otherwise noted.

Electrical Characteristics

At $T_A = +25^\circ\text{C}$ and $R_L = 2\text{ k}\Omega$

AUDIO PERFORMANCE	PARAMETER	UNIT
THD+N	Open-loop voltage gain	dB
IMD	Voltage output	V
	Output current	mA
	Open-loop output impedance	Ω
	Short-circuit current	mA
	Capacitive load drive	V
	Specified voltage	V
	Quiescent current (per channel)	mA
	I_Q over Temperature ⁽¹⁾	mA
	Specified range	mA
	Operating range	mA
	Thermal resistance, junction to ambient	$^\circ\text{C}/\text{W}$
	(3) Specified by design and characterization	

OFFSET VOLTAGE

V_{OS}	Input offset voltage	mV
dV_{OS}/dT	V_{OS} over temperature ⁽²⁾	mV/°C
PSRR	Power-supply rejection ratio	dB

INPUT BIAS CURRENT

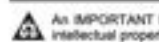
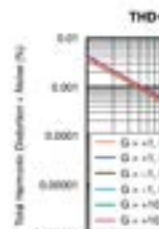
I_B	Input bias current	nA
I_B over temperature ⁽²⁾		nA/°C
I_{OS}	Input offset current	nA

INPUT VOLTAGE RANGE

V_{CM}	Common-mode voltage range	V
CMRR	Common-mode rejection ratio	dB

INPUT IMPEDANCE

	Differential	Ω
	Common-mode	Ω



- (1) Full-power bandwidth = $SR / (2\pi \times V_P)$, where V_P is the peak-to-peak output voltage.
- (2) Specified by design and characterization.

6.5 Typical Char

At $T_A = +25^\circ\text{C}$, $V_S =$

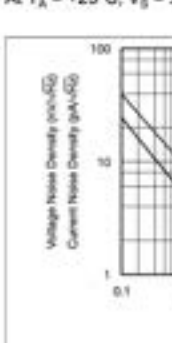


Figure 1. Input

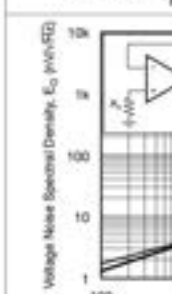
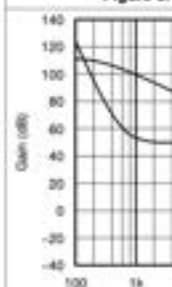


Figure 3.



Figure

OPA1611, OPA

SBOS490C – JULY 2009 – REVISED AUGUST 2014

7 Detailed I

7.1 Overview

The OPA161x is an ultralow-noise, high-slew-rate, rail-to-rail output operational amplifier. It is designed for high-fidelity audio applications. The device has a quiescent current of $\pm 40\text{ mA}$ and a unity-gain bandwidth of 10 MHz .

7.2 Function

OPA1611, OPA1612

SBOS490C – JULY 2009 – REVISED AUGUST 2014

10 Layout

10.1 Layout Guidelines

- For best operational performance of the device, use good printed circuit board (PCB) layout practices, including:
- Noise can propagate into analog circuitry through the power pins of the circuit as a whole and the op amp itself. Bypass capacitors are used to reduce the coupled noise by providing low-impedance power sources local to the analog circuitry.
 - Connect low-ESR, $0.1\text{-}\mu\text{F}$ ceramic bypass capacitors between each supply pin and ground, placed as close to the device as possible. A single bypass capacitor from $V+$ to ground is applicable for single-supply applications.
 - Separate grounding for analog and digital portions of the circuitry is one of the simplest and most-effective methods of noise suppression. One or more layers on multilayer PCBs are usually devoted to ground planes. A ground plane helps distribute heat and reduces EMI noise pickup. Make sure to physically separate digital and analog grounds while paying attention to the flow of the ground current. For more detailed information, refer to the application report *Circuit Board Layout Techniques* (SLOA089).
 - In order to reduce parasitic coupling, run the input traces as far away from the supply or output traces as possible. If these traces cannot be kept separate, crossing the sensitive trace perpendicular as opposed to in parallel with the noisy trace is the preferred method.
 - Place the external components as close to the device as possible. As shown in Figure 36, keeping RF and RG close to the inverting input minimizes parasitic capacitance.
 - Keep the length of input traces as short as possible. Always remember that the input traces are the most sensitive part of the circuit.
 - Consider a driven, low-impedance guard ring around the critical traces. A guard ring can significantly reduce leakage currents from nearby traces that are at different potentials.

10.2 Layout Example

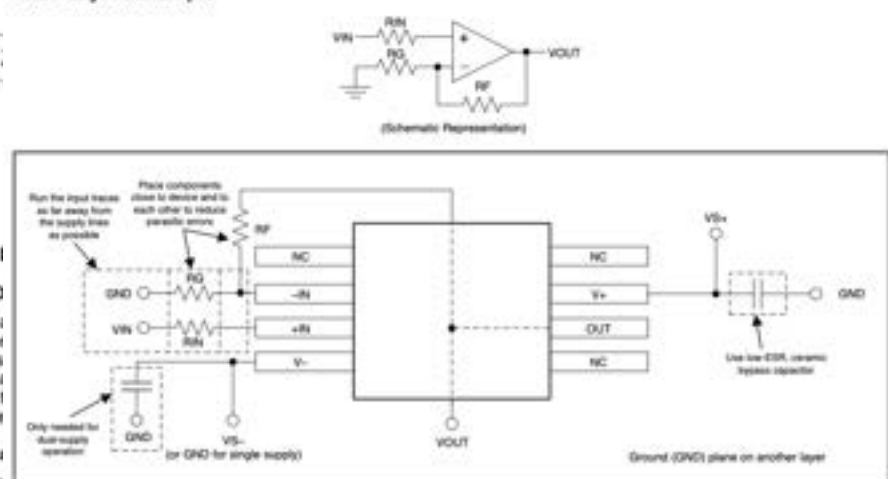


Figure 36. Operational Amplifier Board Layout for a Noninverting Configuration

DISCRETE VS INTEGRATED

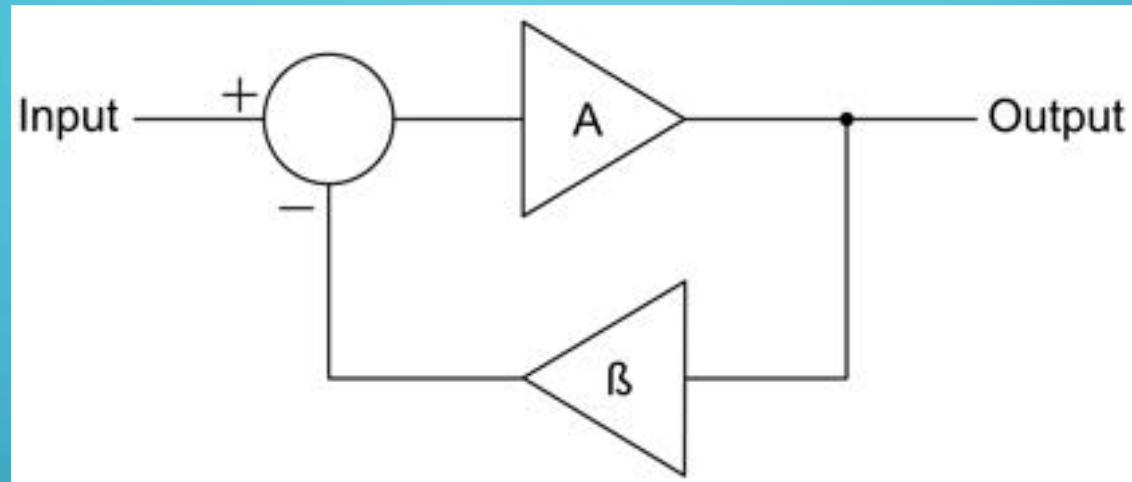
DISCRETE (DUAL)

- Sparkos SS3602: \$79.80
- Staccato OSH-DHA: \$89.00
- Burson V7 Pro, Vivid: \$89.28

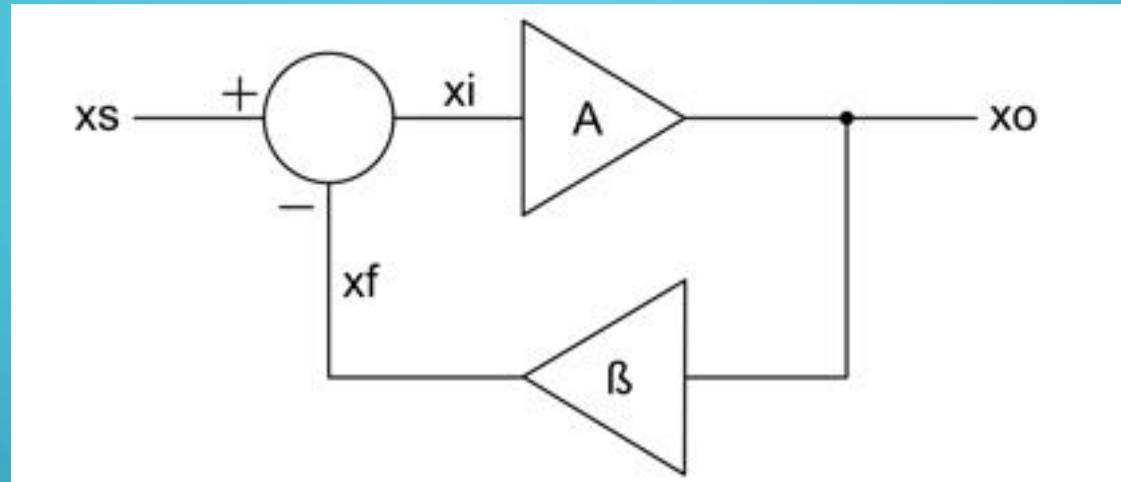
INTEGRATED (DUAL) – QTY 1 (Mouser)

- TI OPA1642AIDR: \$2.10
- TI LME49720NA/NOPB: \$3.69
- TI OPA1612AIDR: \$6.59

STABILITY ANALYSIS



STABILITY ANALYSIS

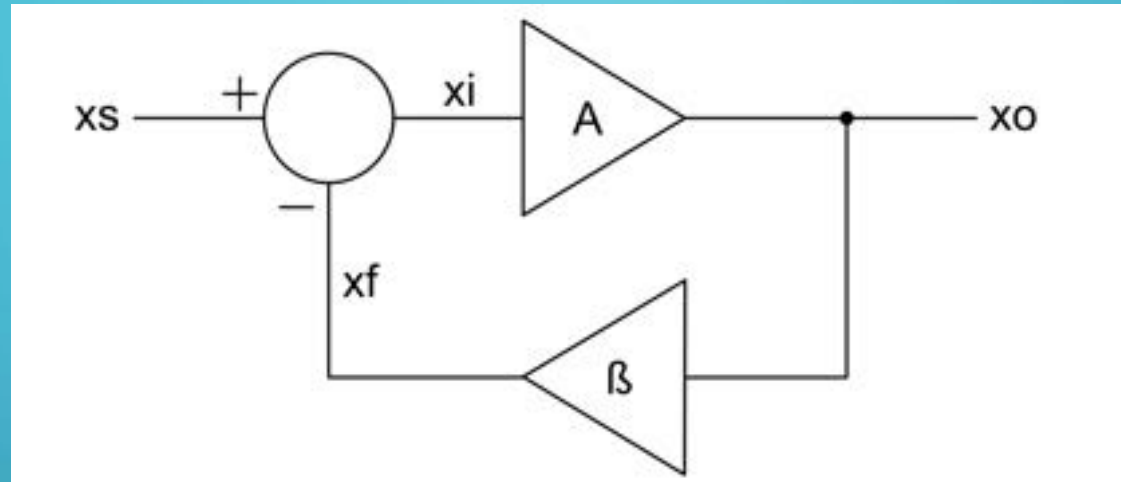


$$x_o = A \cdot x_i$$

$$x_f = \beta \cdot x_o$$

$$x_i = x_s - x_f$$

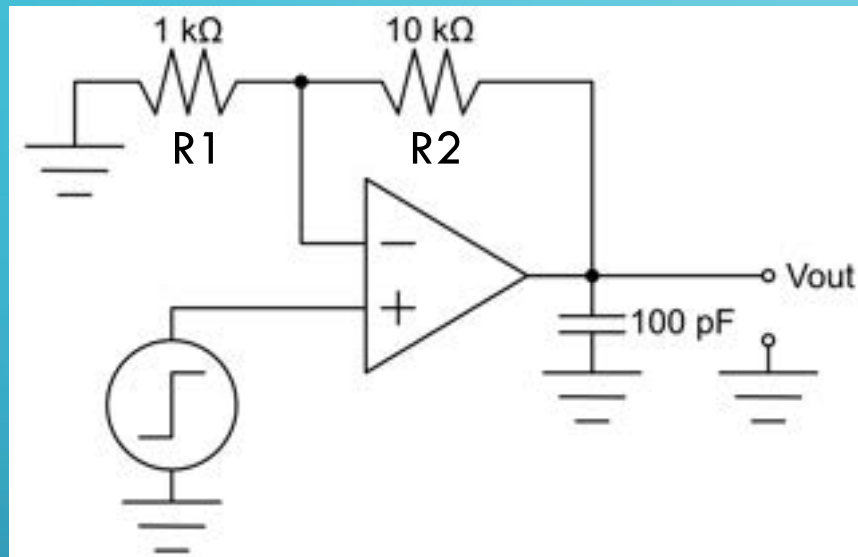
STABILITY ANALYSIS



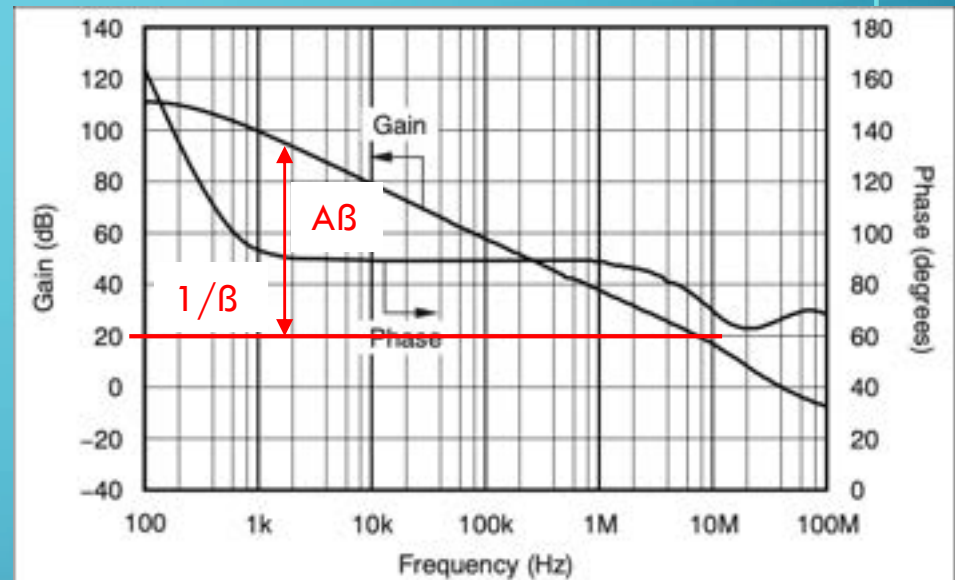
$$A_{CL} = \frac{x_o}{x_s} = \frac{A}{1 + A\beta}$$

$$\text{For } A\beta \gg 1 \quad A_{CL} \approx \frac{1}{\beta}$$

REAL WORLD EXAMPLE I – GAIN STAGE



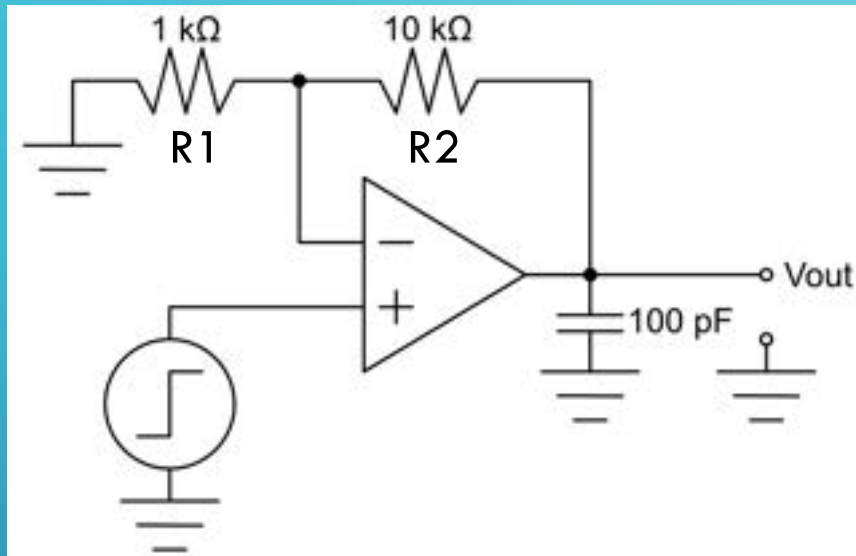
$$\beta = \frac{R1}{R1 \cdot R2} = \frac{1}{10}$$



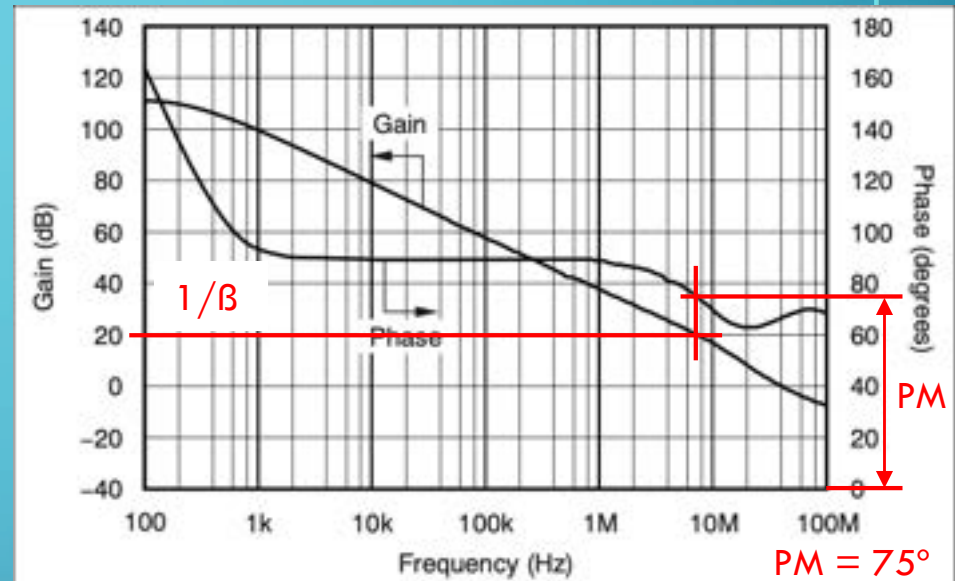
OPA1612

Figure 5. Gain and Phase vs Frequency

REAL WORLD EXAMPLE I – GAIN STAGE

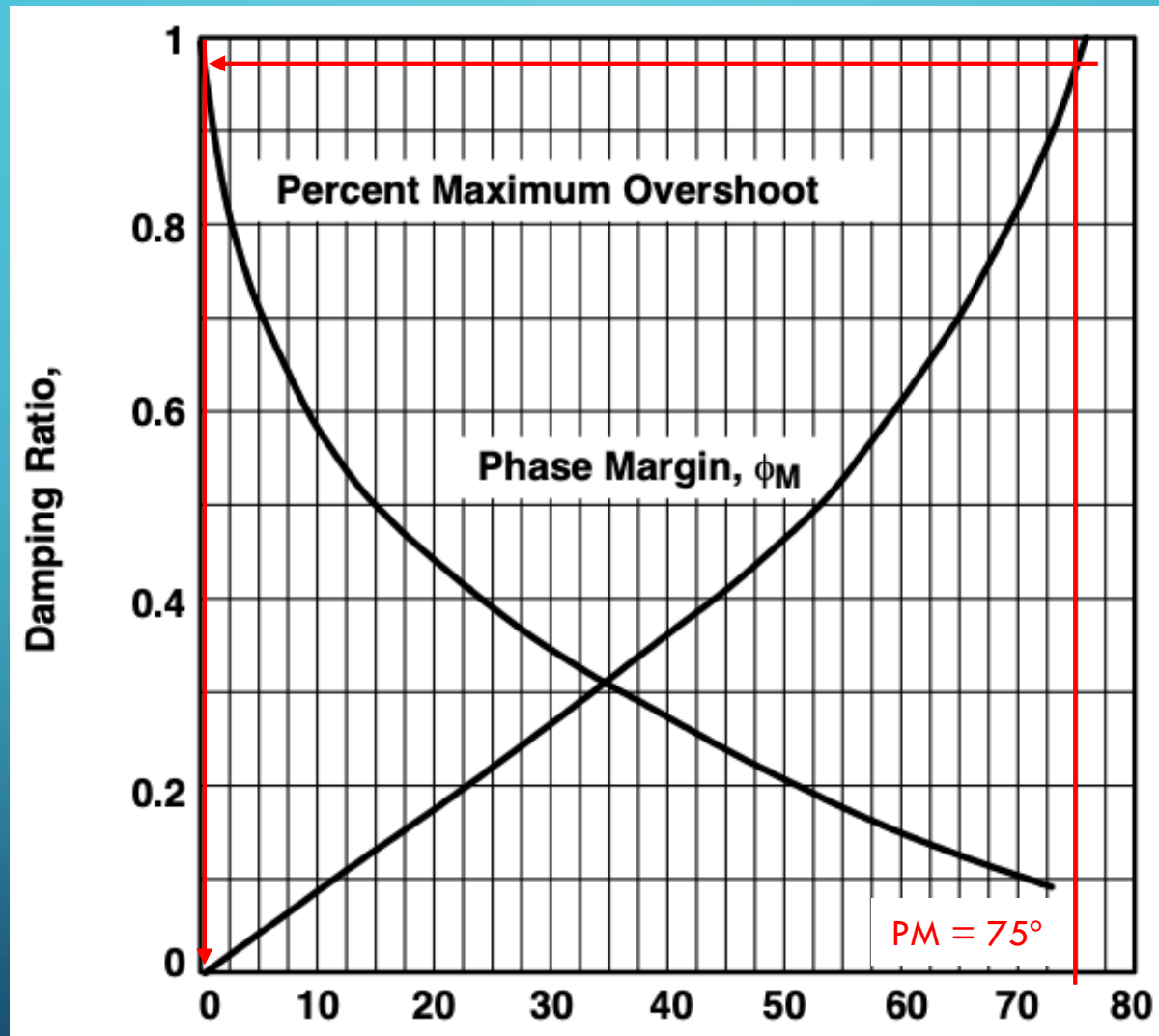


$$\beta = \frac{R1}{R1 \cdot R2} = \frac{1}{10}$$



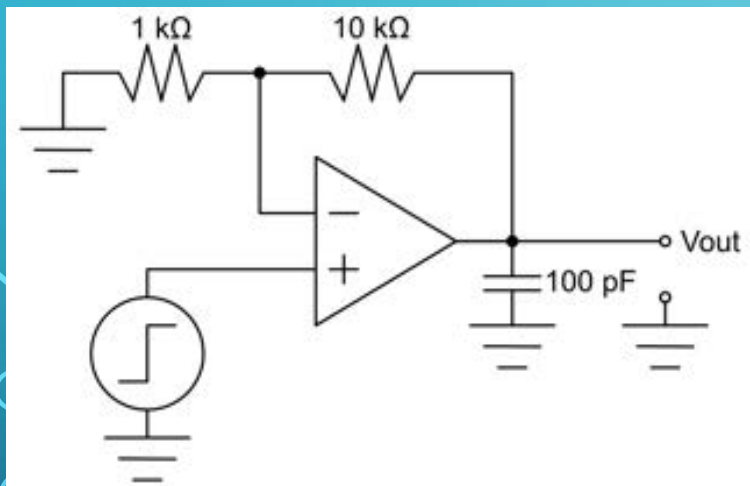
OPA1612 Figure 5. Gain and Phase vs Frequency

REAL WORLD EXAMPLE I – GAIN STAGE

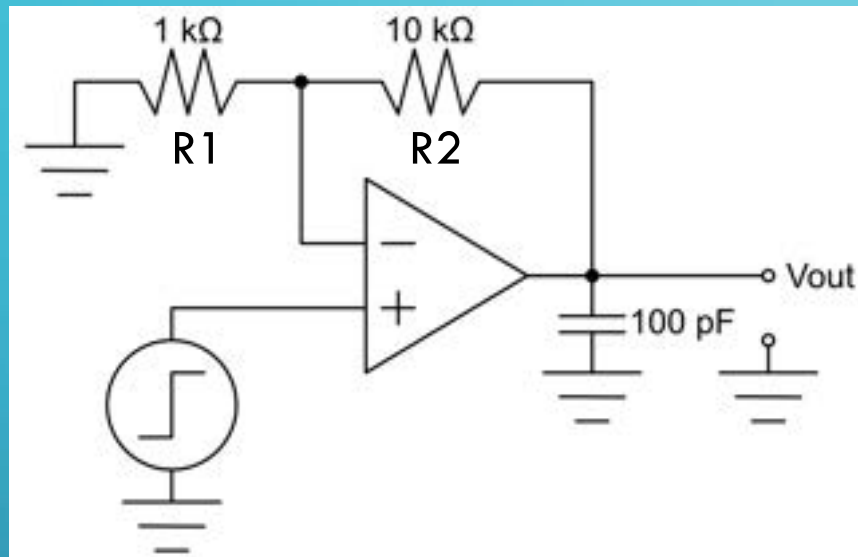


(TI: Opamps for Everyone, Fig. 5-18)

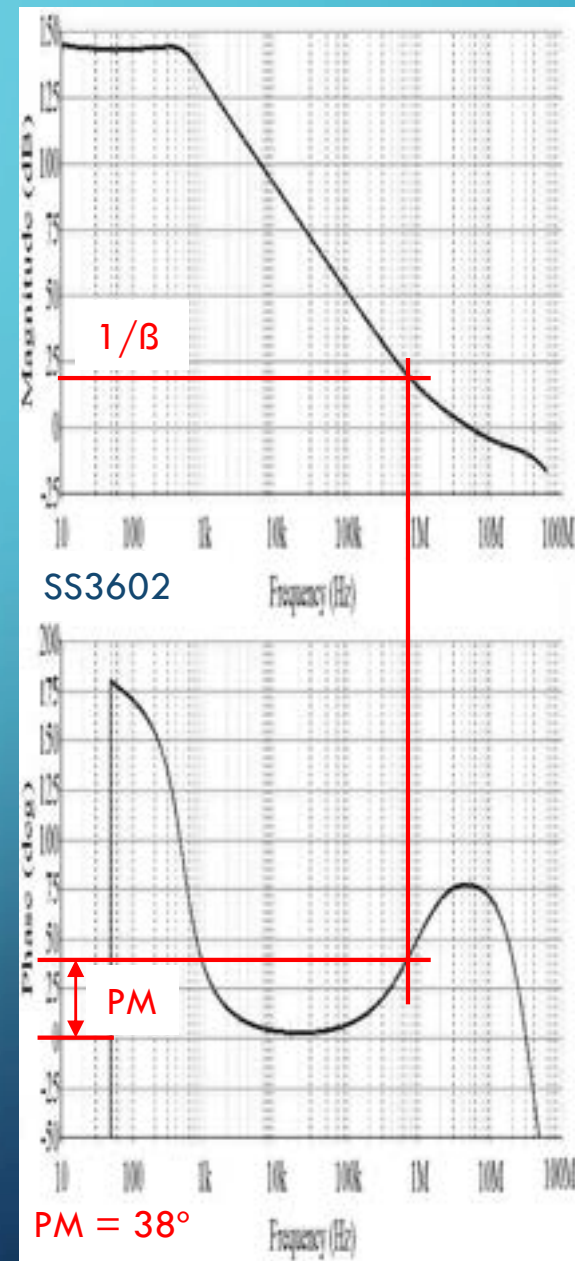
REAL WORLD EXAMPLE I – GAIN STAGE



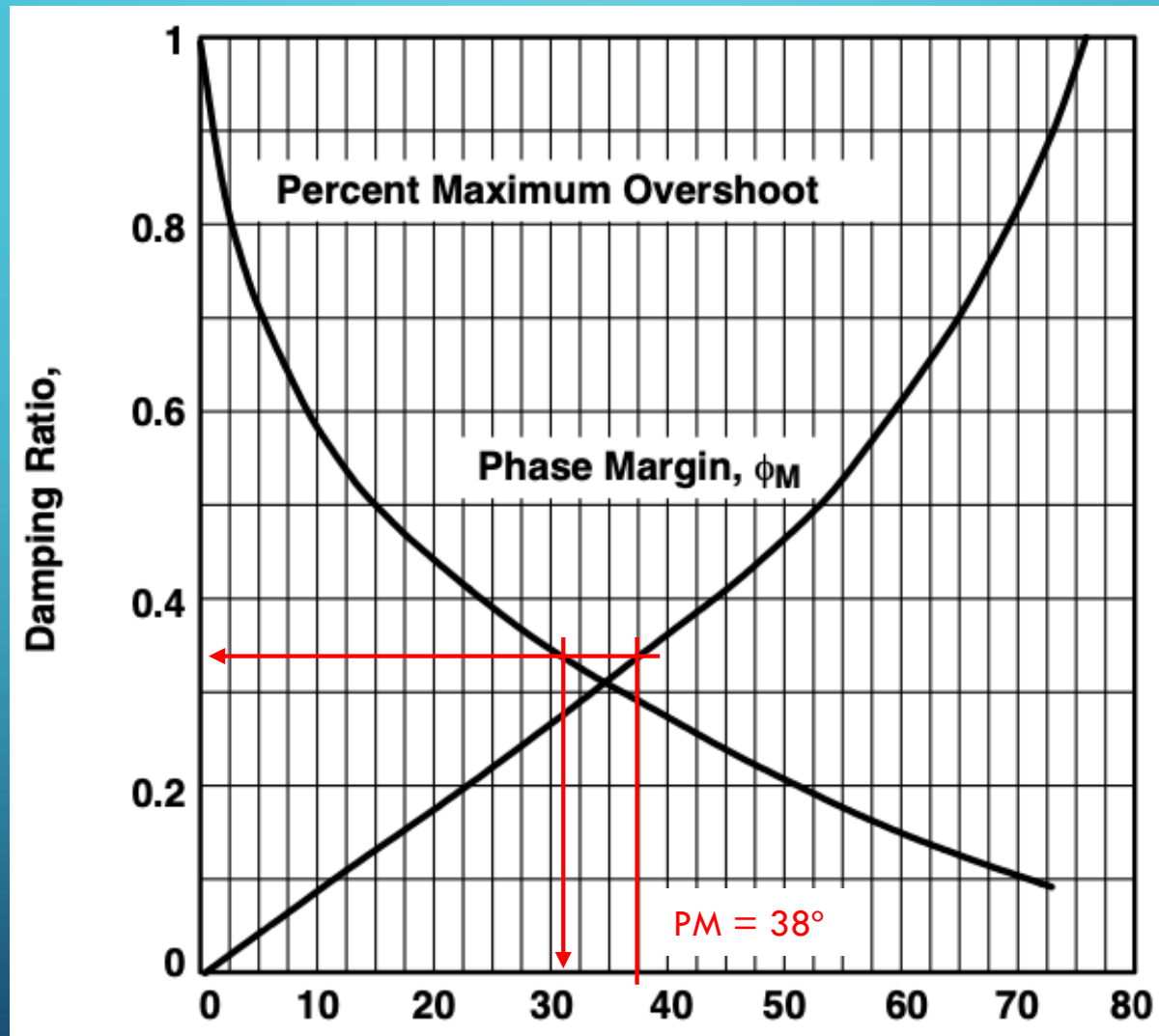
REAL WORLD EXAMPLE I – GAIN STAGE



$$\beta = \frac{R1}{R1 \cdot R2} = \frac{1}{10}$$

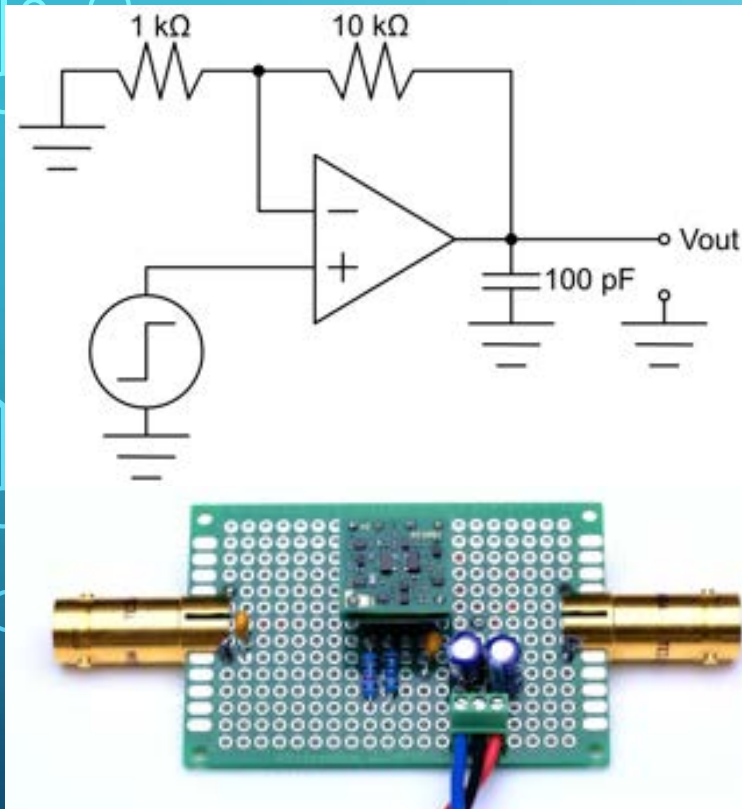


REAL WORLD EXAMPLE I – GAIN STAGE

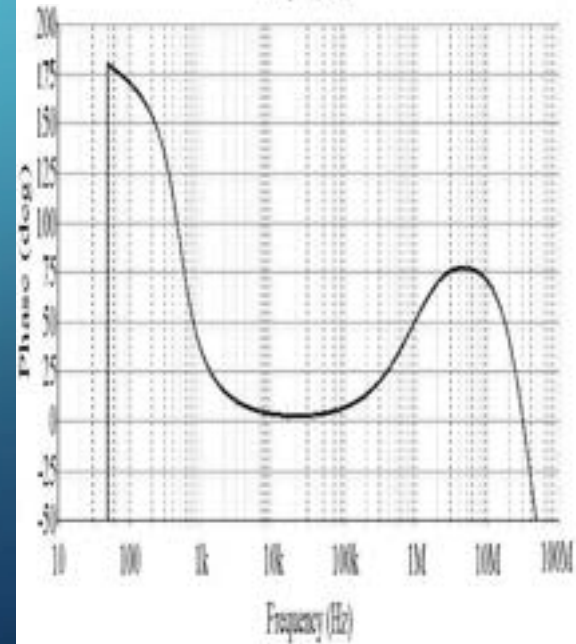
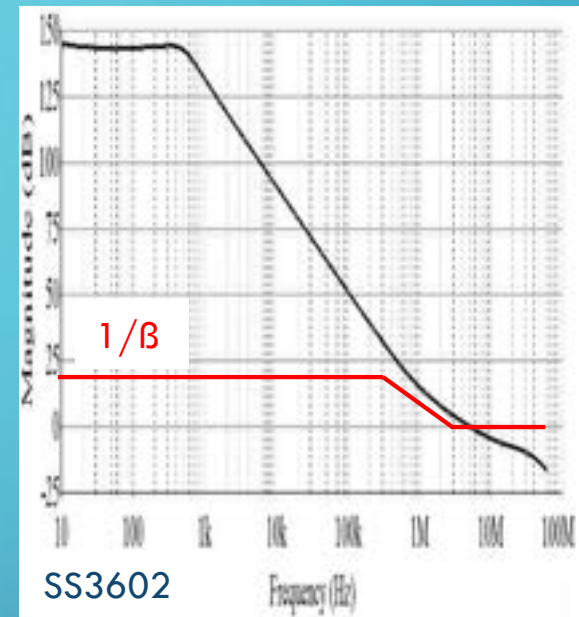
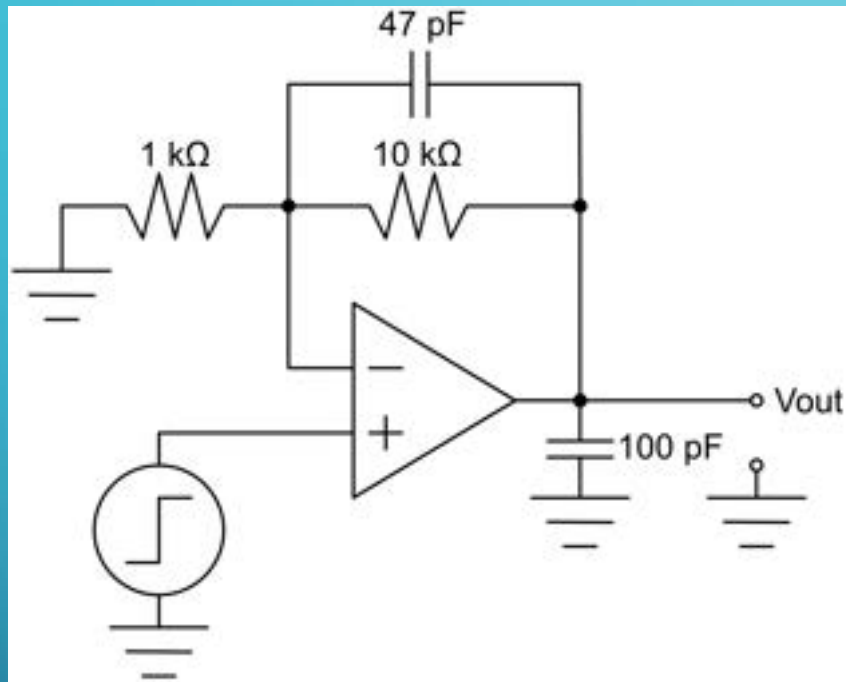


(TI: Opamps for Everyone, Fig. 5-18)

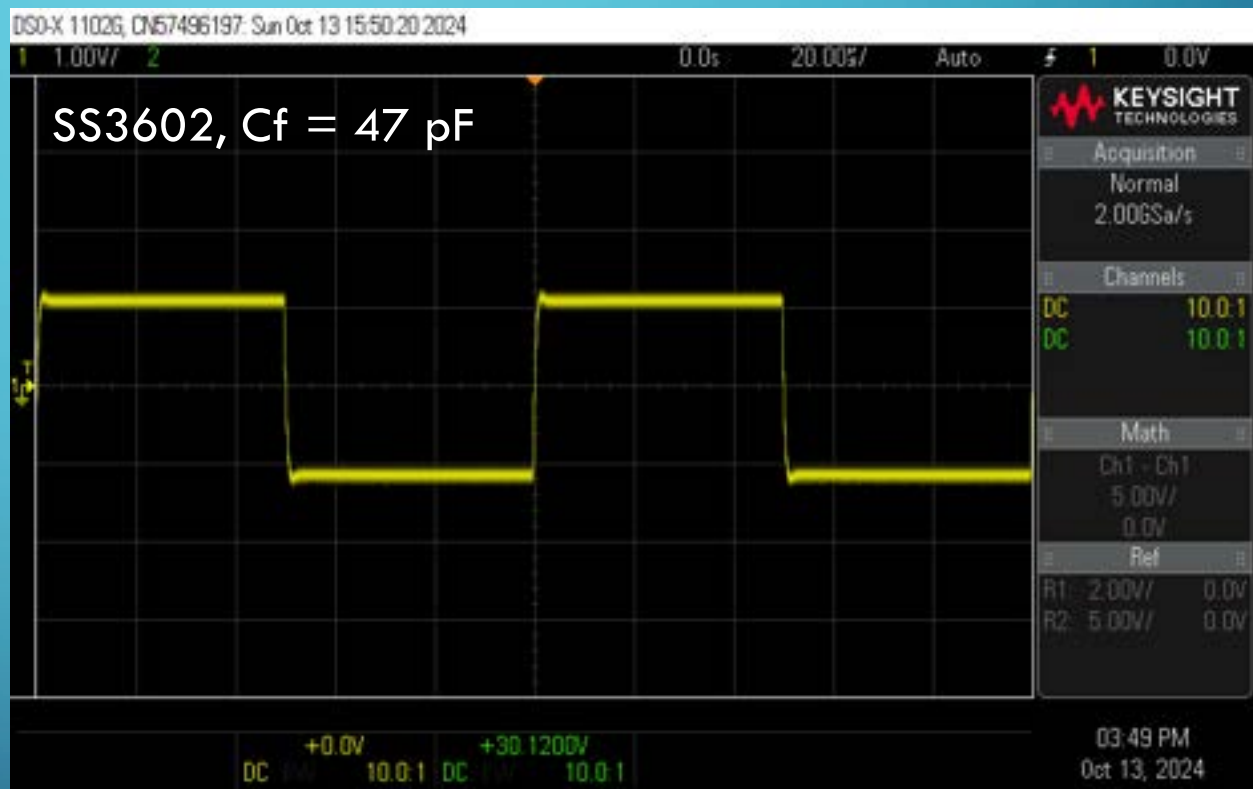
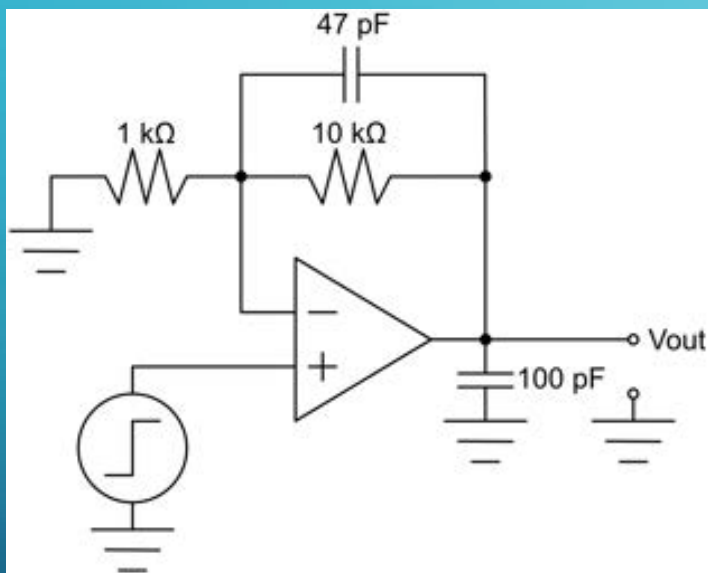
REAL WORLD EXAMPLE I – GAIN STAGE



REAL WORLD EXAMPLE I – GAIN STAGE



REAL WORLD EXAMPLE I – GAIN STAGE



REAL WORLD EXAMPLE I – GAIN STAGE

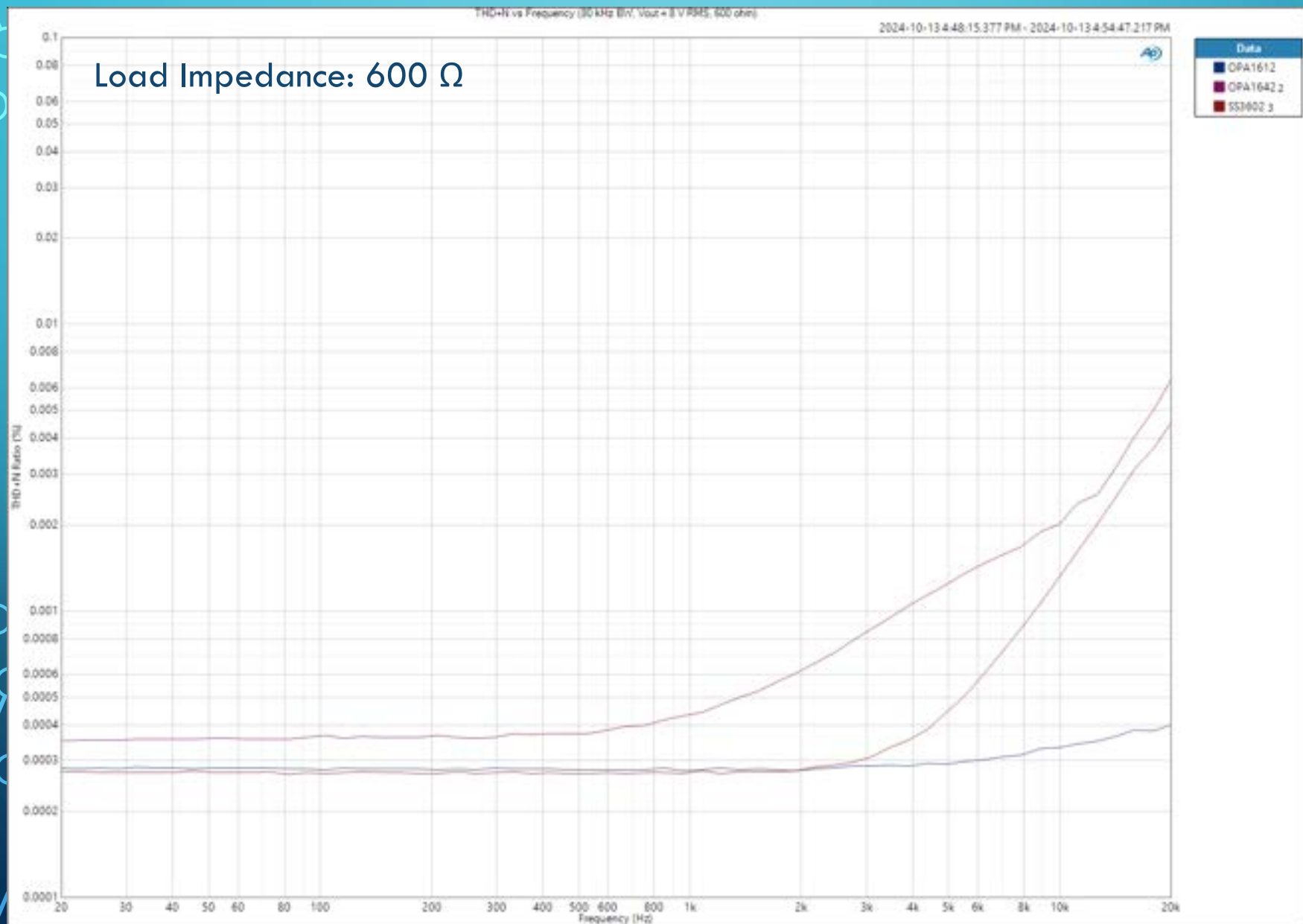


REAL WORLD EXAMPLE I – GAIN STAGE

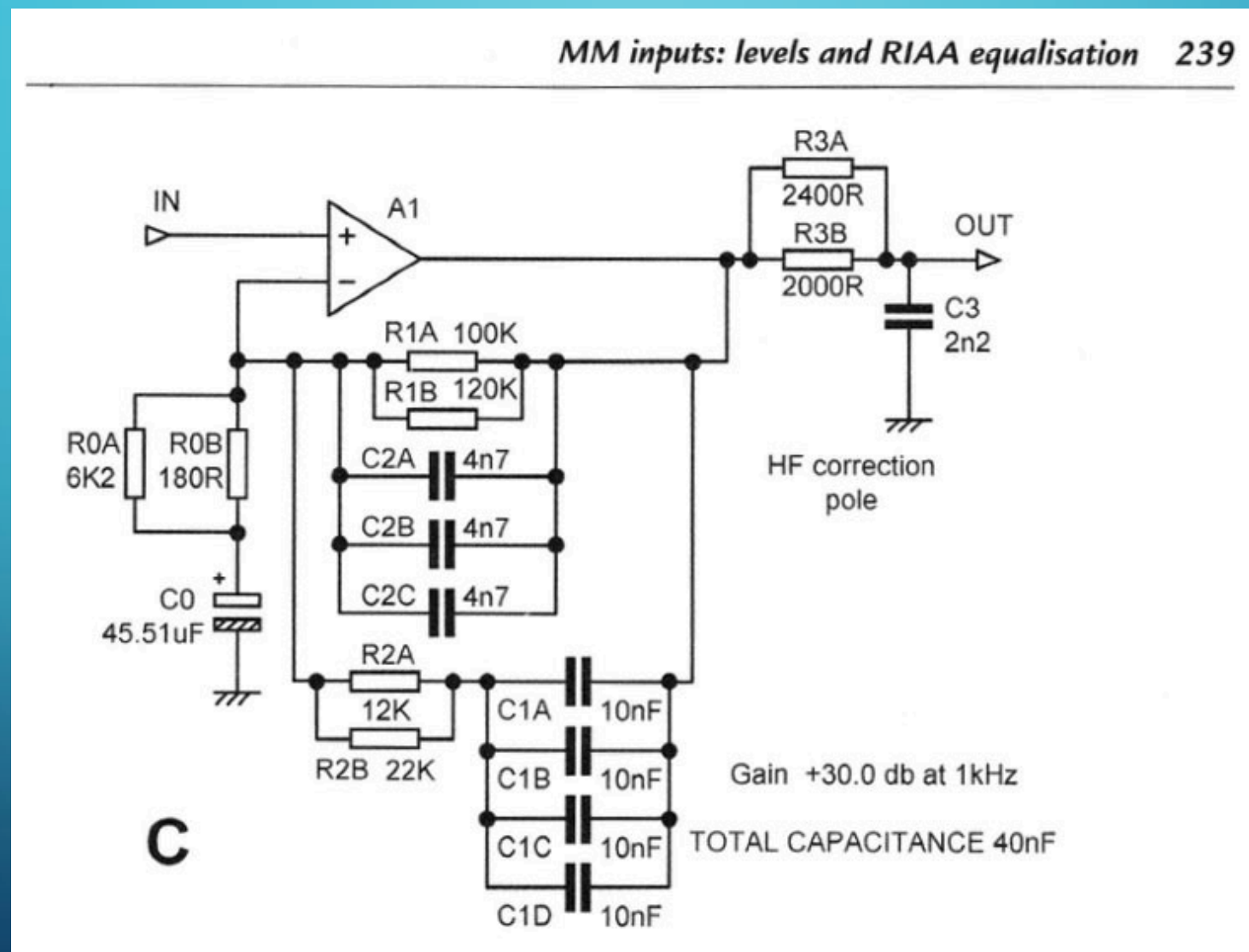


REAL WORLD EXAMPLE I – GAIN STAGE

Load Impedance: 600 Ω

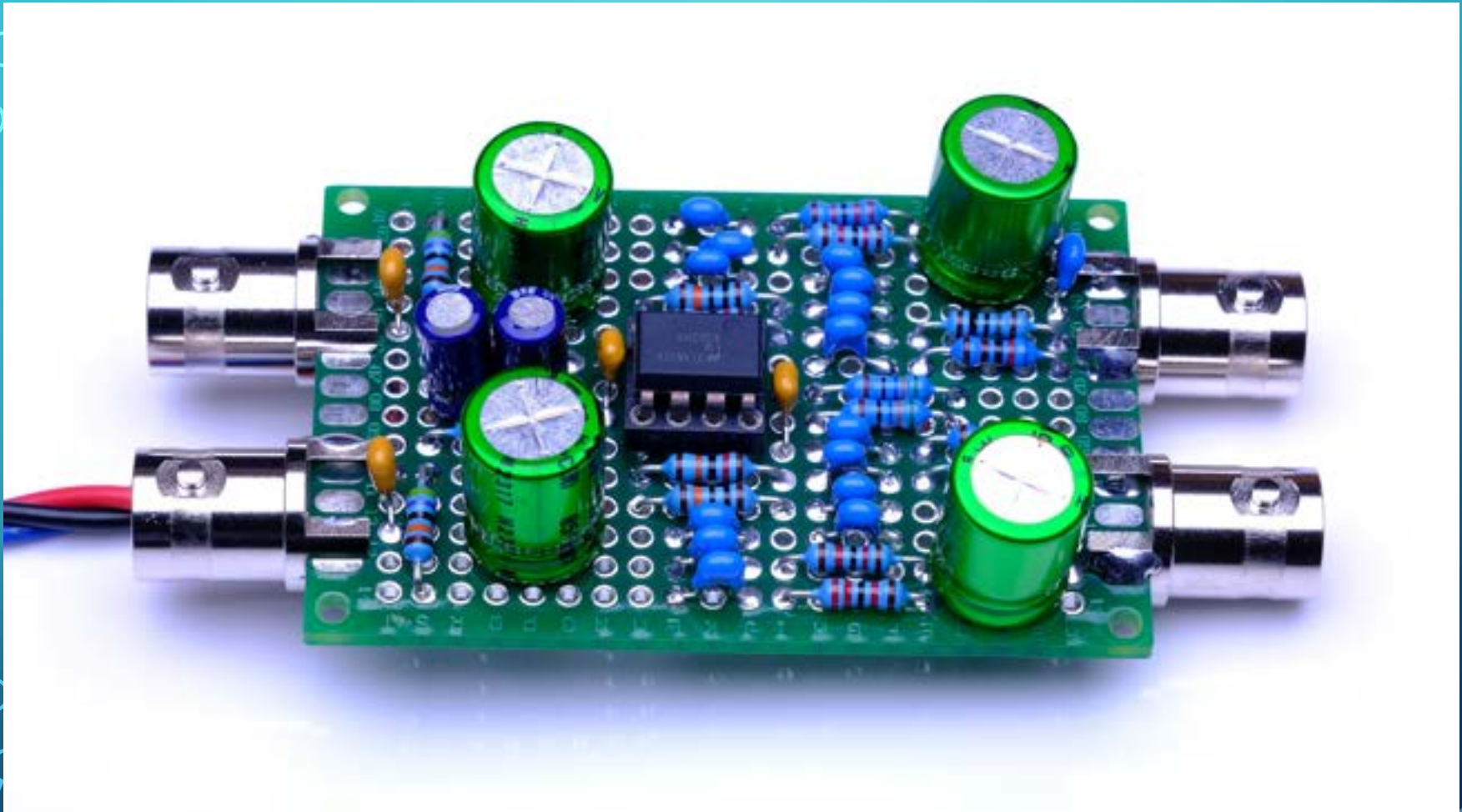


REAL WORLD EXAMPLE II – PHONO STAGE

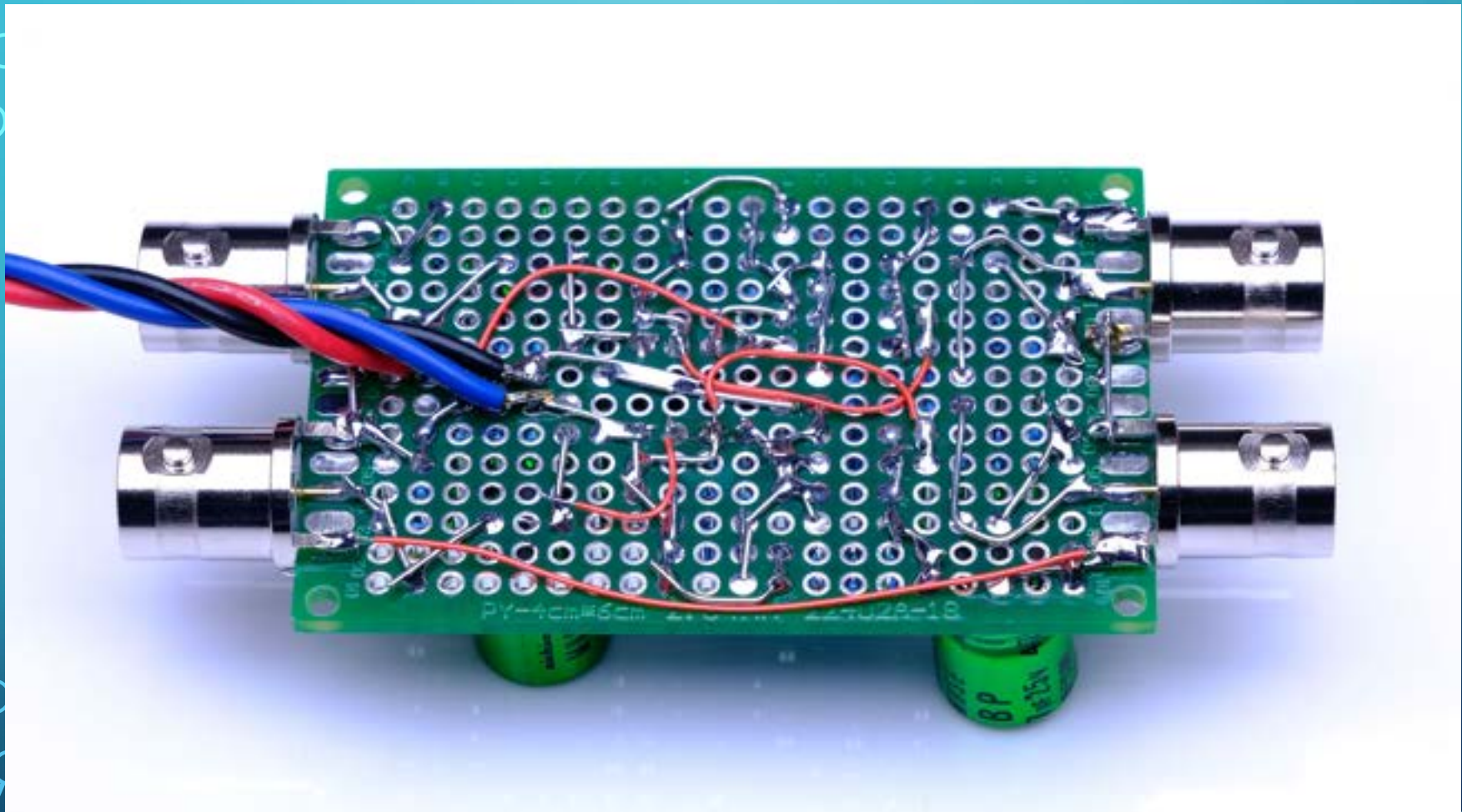


(Self (2014) *Small Signal Audio Design*, 2nd Ed)

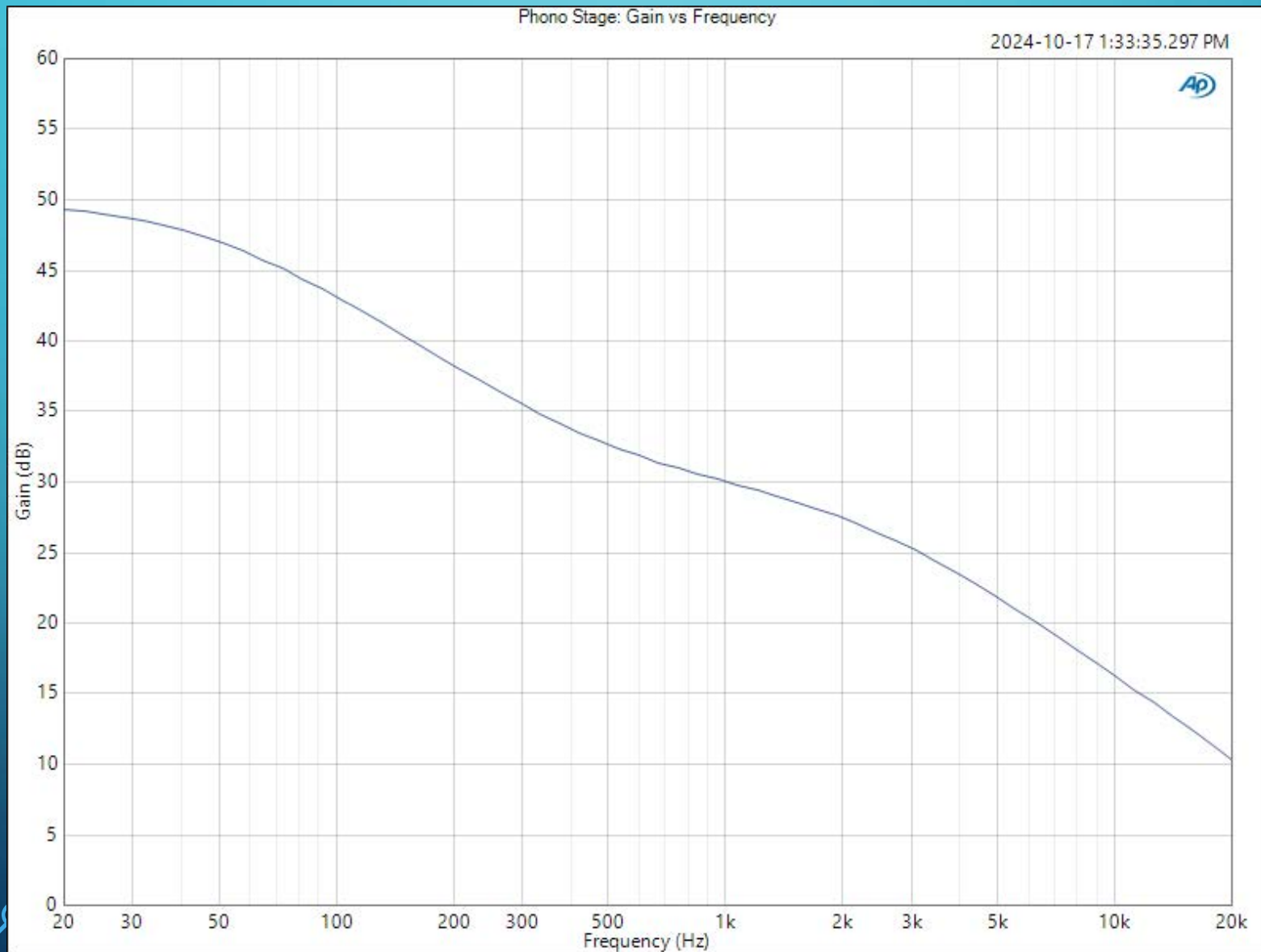
REAL WORLD EXAMPLE II – PHONO STAGE



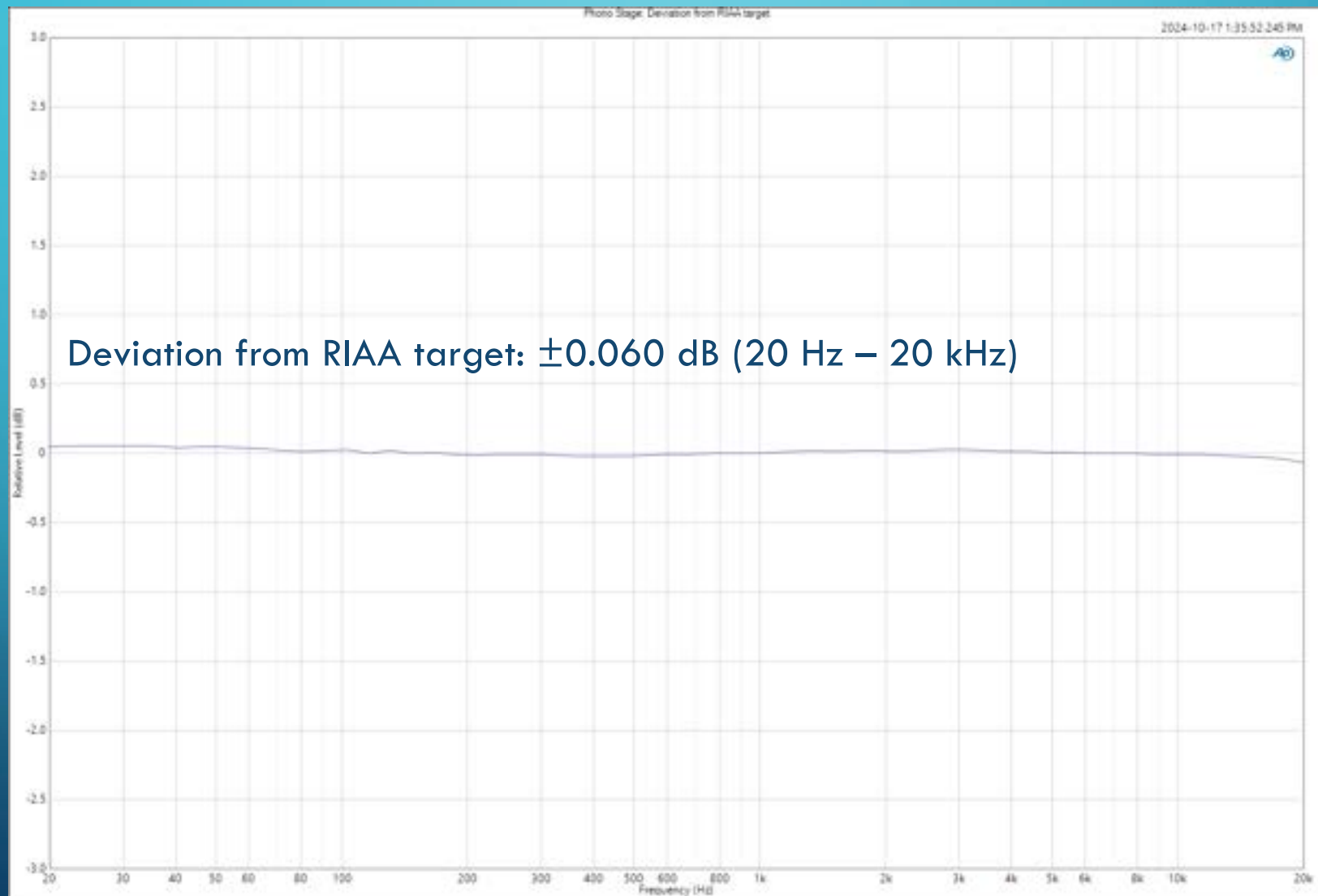
REAL WORLD EXAMPLE II – PHONO STAGE



REAL WORLD EXAMPLE II – PHONO STAGE



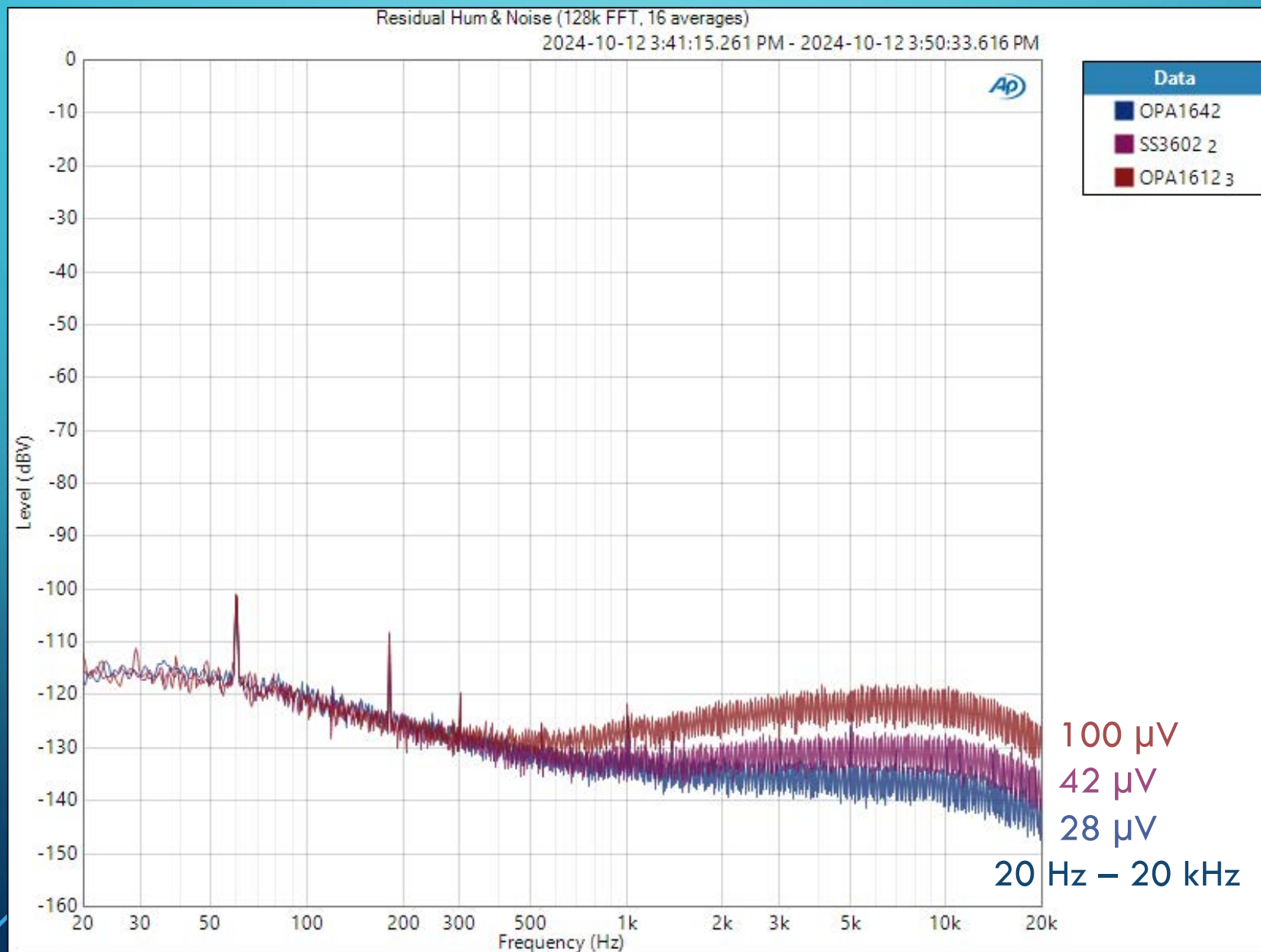
REAL WORLD EXAMPLE II – PHONO STAGE



REAL WORLD EXAMPLE II – PHONO STAGE



REAL WORLD EXAMPLE II – PHONO STAGE



REAL WORLD EXAMPLE II – PHONO STAGE

OPA1612

NOISE				
	Input voltage noise	f = 20 Hz to 20 kHz	1.2	μV_{PP}
e_n	Input voltage noise density ⁽²⁾	f = 10 Hz	2	nV/\sqrt{Hz}
		f = 100 Hz	1.5	nV/\sqrt{Hz}
		f = 1 kHz	1.1	1.5 nV/\sqrt{Hz}
i_n	Input current noise density	f = 10 Hz	3	pA/\sqrt{Hz}
		f = 1 kHz	1.7	pA/\sqrt{Hz}

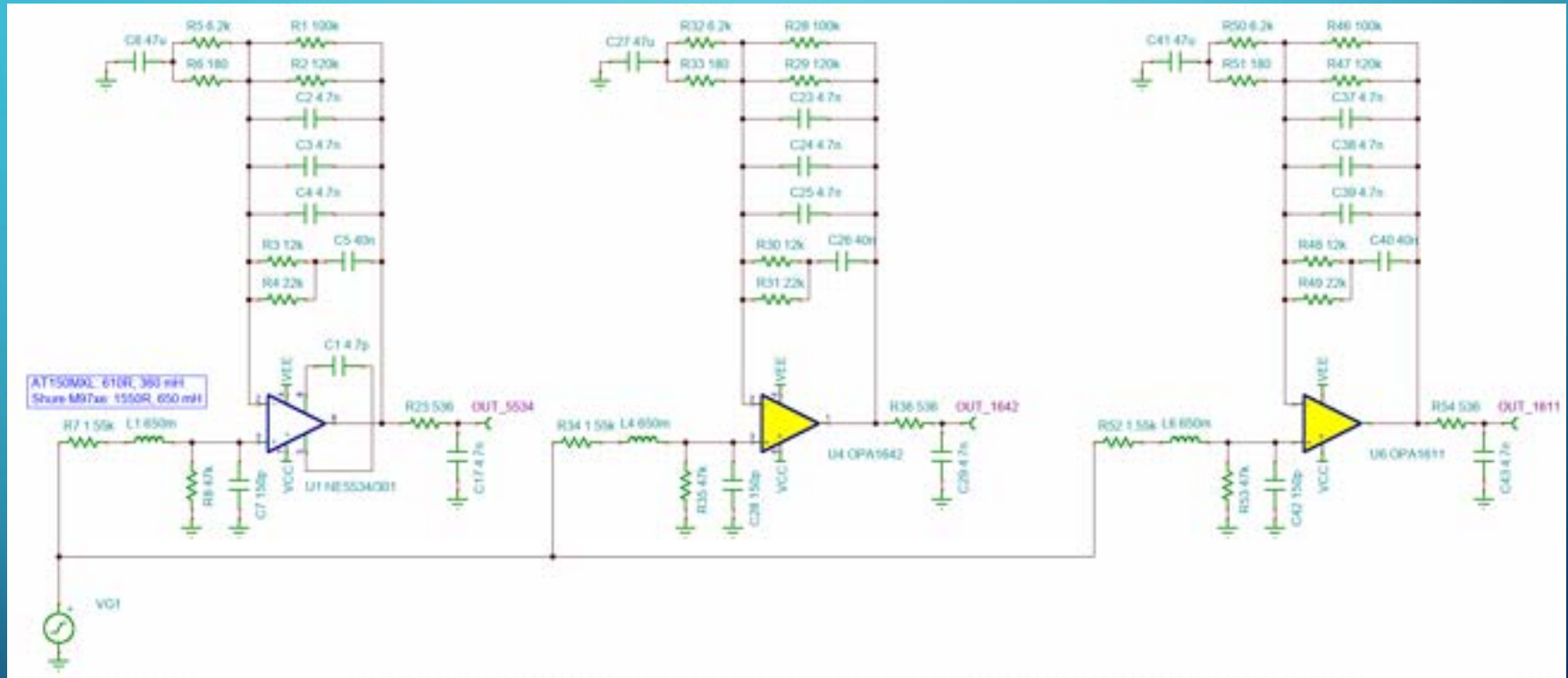
OPA1642

NOISE				
	Input voltage noise	f = 20 Hz to 20 kHz	4.3	μV_{PP}
e_n	Input voltage noise density	f = 10 Hz	8	nV/\sqrt{Hz}
		f = 100 Hz	5.8	
		f = 1 kHz	5.1	
i_n	Input current noise density	f = 1 kHz	0.8	fA/\sqrt{Hz}

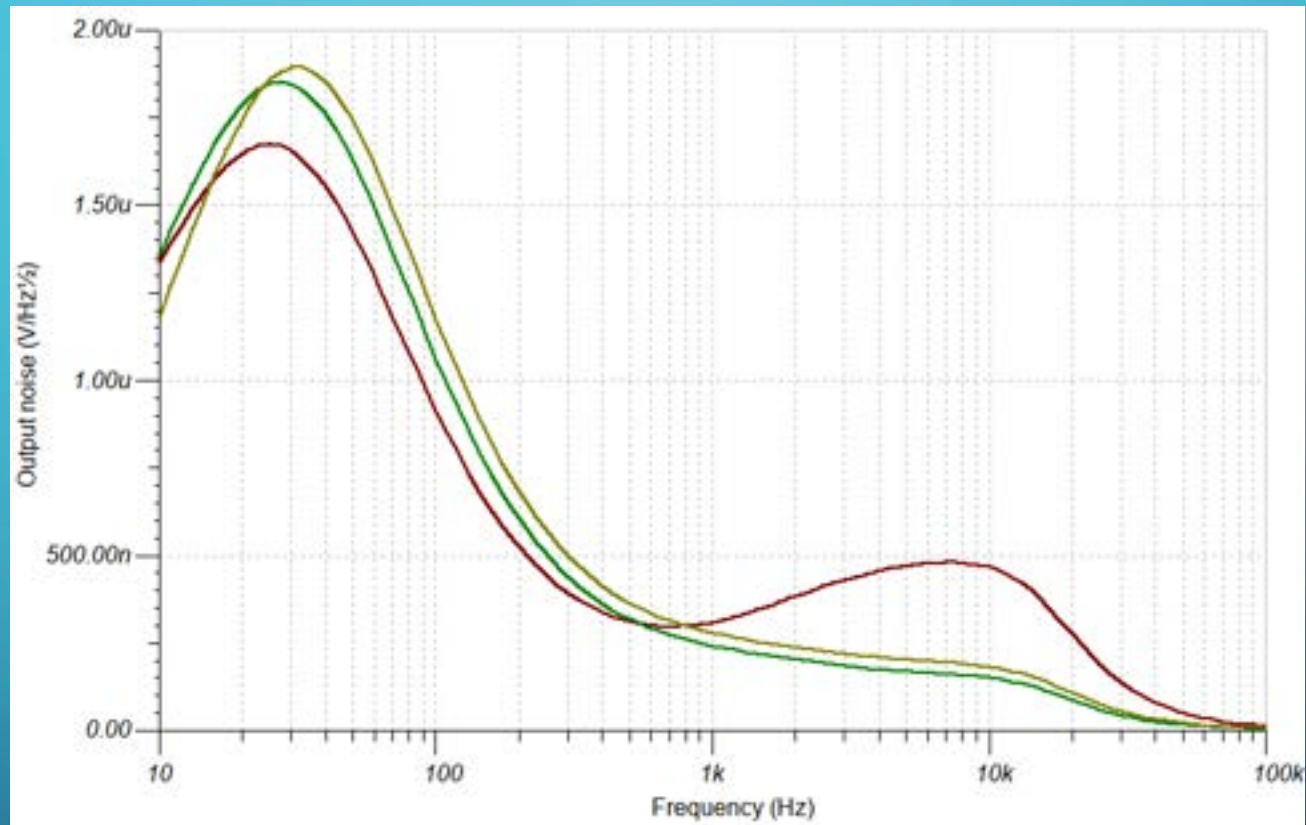
NE5534

V_n	Equivalent input noise voltage	f = 30 Hz	7	5.5	7	nV/\sqrt{Hz}
		f = 1 kHz	4	3.5	4.5	
i_n	Equivalent input noise current	f = 30 Hz	2.5	1.5		pA/\sqrt{Hz}
		f = 1 kHz	0.6	0.4		

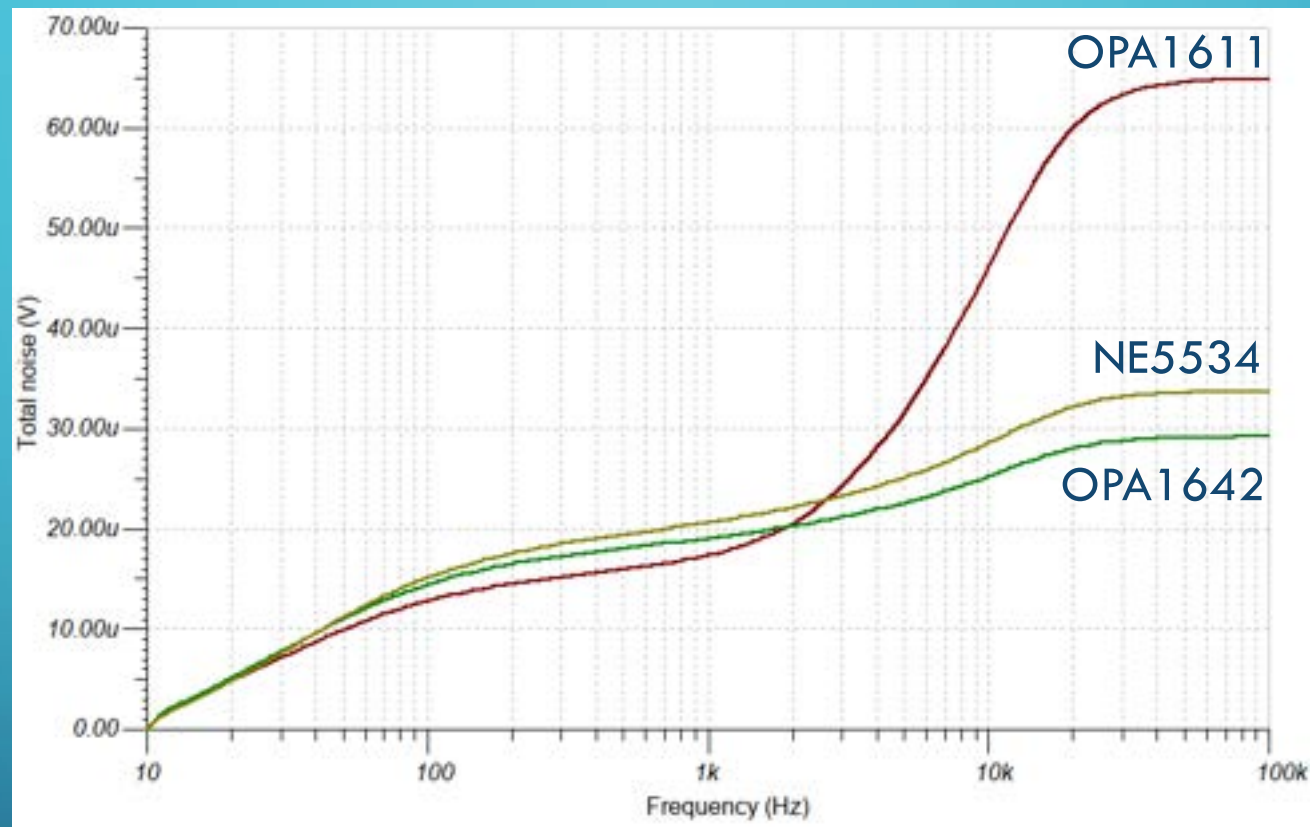
REAL WORLD EXAMPLE II – PHONO STAGE



REAL WORLD EXAMPLE II – PHONO STAGE



REAL WORLD EXAMPLE II – PHONO STAGE



LESSONS LEARNED

- Mind the stability, especially with discrete opamps
- More expensive is not always better
- Choose an opamp appropriate for the application
- Opamp rolling changes circuit performance ... but not always for the better

QUESTIONS



(The Atlantic)