

Electrical Parameters

$$\Delta\beta_m := 0.32T$$

Peak Operating Flux Density for the transformer Tesla

$$F_{sw} := 20KHz$$

Switching Frequency

$$I_{pRMS} := 5A$$

$$P_{in} := 5W$$

Find the size of core Required

$$CM := 0.000005067cm^2$$

$$J_{density} := 500 \frac{A}{cm^2}$$

Suggested Wire current density. 300 is very conservative, 500 is normal (often used for continuous power), 800 is high but is often used as the peak power number

$$D_{cma} := \frac{m^2}{J_{density} \cdot CM}$$

$$K_t := 100$$

Kt = 100 Push Pull
Kt = 140 Half Bridge
Kt = 140 Full Bridge
Kt = 50 Forward Converter
Kt = 33 Flyback (Single Winding)
Kt = 25 Flyback (Multiple Winding)

$$A_{pRequired} := \frac{P_{in} \cdot D_{cma}}{K_t \cdot \Delta\beta_m \cdot F_{sw} \cdot 10^7}$$

$$A_{pRequired} = 0.031 \cdot cm^4$$

**Core Parameters EE2005S Cosmo
CF139**

$$Ac := 0.335 \text{ cm}^2$$

Core cross sectional winding area

$$MPL := 4.49 \text{ cm}$$

Magnetic Path Length from core data sheet

$$MLT := 3.64 \text{ cm}$$

Mean Length per Turn from bobbin data sheet

$$Vol_{fe} := 0.00 \text{ cm}^3$$

Core Fe Volume

$$CoreWid := 2 \text{ cm}$$

Core Width (C)

$$CoreLen := 0.59 \text{ cm}$$

Core Length (2B)

$$CoreHt := 2.04 \text{ cm}$$

Core Height (A)

$$WindowWidth := 1.4 \text{ cm}$$

Winding Window Width (2F)

$$WindowHt := 0.4 \text{ cm}$$

Window Winding Height (D-E)/2

$$\mu := 2100$$

Core Permeability

$$Wa := WindowWidth \cdot WindowHt$$

Window Area

$$Wa = 0.56 \cdot \text{cm}^2$$

$$UseableWindow := Wa \cdot 0.29 = 0.162 \cdot \text{cm}^2$$

$$BobbinWidth := WindowWidth - 2.2 \text{ mm}$$

Use this equation or enter from bobbin mfg datasheet. Use 2.2mm when using tripple insulated wire and 8.2mm when using margin tape.

$$BobbinWidth = 1.18 \cdot \text{cm}$$

$$Ap := Wa \cdot Ac$$

$$Ap = 0.188 \cdot \text{cm}^4$$

Power Handling ability of the core

$$At := 2 \cdot CoreLen \cdot CoreWid + 2 \cdot CoreLen \cdot CoreHt + 2 \cdot CoreWid \cdot CoreHt$$

$$At = 12.927 \cdot \text{cm}^2$$

Surface Area for heat dissipation
For EE/ER style transformers use the above but substitute for Core Height the following:
CoreHt+2*WindowHt

Constants

$$K_i := 0.0388$$

$$K_w := 0.866$$

$$K_u := 0.29$$

$$K_f := 4$$

Gap Loss Coefficient

Winding factor

Window utilization factor use 40% for most cases

Waveform coefficient use 4 for a square wave or 4.4 for a sinewave

Coil Calculations

$$I_{pk} := 7A$$

Peak Current through the Coil

$$I_{rms} := \sqrt{(2 \cdot I_{pk})^2} = 14A$$

$$L_p := 33\mu H$$

Primary Side Inductance

$$N_p := \frac{I_{pk} \cdot L_p}{\Delta\beta_m \cdot A_c}$$

Adjust ΔI and $\Delta\beta_m$ above to get a whole number for N_p

$$N_p = 21.549$$

$$N_p := 22$$

$$l_g := 0.94mm$$

$$FFlux := 1 + \frac{l_g}{\sqrt{A_c}} \cdot \ln\left(\frac{2 \cdot WindowWidth}{l_g}\right)$$

$$FFlux = 1.551$$

$$L_{gapped} := \frac{\left(0.4 \cdot \frac{H}{m} \cdot \pi \cdot 10^{-6}\right) \cdot N_p^2 \cdot FFlux \cdot A_c}{l_g + \frac{MPL}{\mu}}$$

$$L_{\text{gapped}} = 32.876 \cdot \mu\text{H}$$

This needs to equal L_p $L_p = 33 \cdot \mu\text{H}$

$$B_{\text{max}} := \frac{0.4 \frac{\text{H}}{\text{m}} \cdot \pi \cdot N_p \cdot \text{FFlux} \cdot (I_{\text{pk}}) \cdot 10^{-6}}{l_g + \frac{\text{MPL}}{\mu}}$$

$$B_{\text{max}} = 0.312 \text{ T}$$

Double Check this against your input requirement

$$\beta_{\text{ac}} := \frac{0.4 \frac{\text{H}}{\text{m}} \cdot \pi \cdot N_p \cdot \text{FFlux} \cdot \left(\frac{I_{\text{pk}}}{1}\right) \cdot 10^{-6}}{l_g + \frac{\text{MPL}}{\mu}}$$

$$\beta_{\text{ac}} = 0.312 \text{ T}$$

AC Component

$$\beta_{\text{dc}} := B_{\text{max}} - \beta_{\text{ac}}$$

$$\beta_{\text{dc}} = 0 \text{ T}$$

DC component

$$\text{Energy} := \frac{L_p \cdot I_{\text{pk}}^2}{2}$$

Energy in W-S

$$\text{Energy} = 0.000808 \text{ J}$$

$$\text{Power} := \text{Energy} \cdot F_{\text{sw}} = 16.17 \text{ W}$$

Max Power available at that frequency and inductance

$$A_{\text{Le}} := \frac{L_p}{N_p^2 \cdot 10^{-3}}$$

Effective A_{Le} gapped $\mu\text{H}/1000$ turns

$$A_{\text{Le}} = 68 \cdot \mu\text{H}$$

$$\underline{\underline{H}} := \frac{0.4 \cdot \pi \cdot N_p \cdot I_{\text{pk}}}{\text{MPL}}$$

Oersteds

$$H = 43.10069 \cdot \frac{A}{cm}$$

Check this against data sheet curves

$$P_g := K_i \cdot \frac{10^4 W}{(m^2 T^2) Hz} \cdot WindowWidth \cdot lg \cdot F_{sw} \cdot \beta_{ac}^2$$

McLyman - Transformer and Inductor design Handbook

$$P_g = 9.957 \text{ W}$$

Skin Depth and Wire Selection

$$\rho := 1.7241 \cdot 10^{-6} \Omega \cdot cm$$

Nema M1000 pdf

$$\alpha := 0.0039$$

Temperature Compensation for Cu

$$TempW := 90$$

Degree C Operating Wire temperature

$$T_{ambient} := 20$$

Ambient Wire Temperature the Cu constant was derived from

$$\rho_e := \rho \cdot [1 + \alpha \cdot (TempW - T_{ambient})]$$

$$\rho_e = 2.195 \times 10^{-6} \Omega \cdot cm$$

$$K_{cu} := \sqrt{\frac{\rho_e}{\rho}}$$

$$\delta := \frac{6.62}{\sqrt{F_{sw}}} \cdot K_{cu} \cdot \sqrt{Hz} \cdot cm$$

$$\delta = 0.053 \cdot cm$$

Skin Depth in cm

$$MaxWireDia := 2\delta$$

$$MaxWireDia = 0.106 \cdot cm$$

Maximum wire Diameter that uses 100% of the Cu area at the fundamental switching frequency

$$MaxWireDia := 0.1cm$$

$$MaxWireOD := 0.12cm$$

Wire Gauge is 18AWG

Primary Side Wire Selection

WireDia := 1.0mm

Bare Cu wire Diameter for the Primary Winding

WireOD := 1.05mm

Uses 2UEW (JIS Grade 2) See wire table

$$\frac{\text{BobbinWidth} \cdot 2}{N_p} = 0.107 \cdot \text{cm}$$

Max wire dia for $N_p/2$ turns

$$\text{MaxTurn} := \text{floor}\left(\frac{\text{BobbinWidth}}{\text{WireOD}}\right)$$

MaxTurn = 11

This is the Maximum Number of turns for single layer construction. Check this value against N_p

$$\text{MaxISWG} := \text{Idensity} \cdot \left(\frac{\text{MaxWireDia}}{2}\right)^2 \cdot \pi$$

MaxISWG = 3.927 A

$$\text{SuggestedNumbStrands} := \frac{\text{Irms}}{\left(\frac{\text{WireDia}}{2}\right)^2 \cdot \pi \cdot \text{Idensity}}$$

SuggestedNumbStrands = 3.565

NumPriStrands := 4

Number of parallel strands of wire to use in the primary winding

$$\text{WindingAreaPri} := \text{Np} \cdot \text{WireDia}^2 \cdot \text{NumPriStrands} \cdot \text{Kw}$$

$$\text{WindingAreaPri} = 76.208 \cdot \text{mm}^2$$

$$\text{AwbWinding} := \pi \cdot \left(\frac{\text{WireDia}}{2} \right)^2 \cdot \text{NumPriStrands} \quad \text{Cross Sectional area of the stranded wire}$$

$$\text{AwbWinding} = 3.142 \cdot \text{mm}^2$$

$$\text{RcuWinding} := \frac{\rho_e}{\text{AwbWinding}} \cdot \text{MLT} \cdot \text{Np} \quad \text{DCR Of the Winding}$$

$$\text{RcuWinding} = 5.595 \times 10^{-3} \Omega$$

$$\text{PcuWinding} := \text{Ipk}^2 \cdot \text{RcuWinding} \quad \text{Power Dissipation of the winding}$$

$$\text{PcuWinding} = 0.274 \text{ W}$$

$$\text{Coilloss} := \text{Pg} + \text{PcuWinding}$$

$$\text{Coilloss} = 10.231 \text{ W}$$

$$\Delta T := \left[\frac{\frac{\text{Coilloss} \cdot 10^3}{\text{W}}}{\left(\frac{\text{At}}{\text{cm}^2} \right)} \right]^{0.833} \quad ^\circ\text{C}$$

Estimated Temperature Rise over Ambient

$$\Delta T = 259.651 \cdot ^\circ\text{C}$$

$$\text{WindingAreaTot} := \text{WindingAreaPri}$$

$$\text{WindingAreaTot} = 0.762 \cdot \text{cm}^2$$

$$\text{UseableWindow} = 0.162 \cdot \text{cm}^2$$

$$\text{PtotLoss} := \text{Coilloss}$$

$$\text{PtotLoss} = 10.231 \text{ W}$$