

# Load impedance and operating points for single-ended triode amplifier stages

## Part Two: Linear Triodes

by Paul Joppa

In Part 1 of this series, I described how the operating point (plate voltage  $E_b$  and current  $I_o$ ) and load resistance  $R_L$  are related. In this part, I will use those observations to look at single-ended amplifier performance for triodes that follow closely the simplest expression for plate current as a function of plate and grid voltages, called "Child's Law". I call these tubes linear because they are capable of higher power output at lower distortion than those that deviate significantly from this behavior. Child's Law states that:

$$I_b = K(E_b + m E_c)^{3/2}$$

In this equation,  $I_b$  is plate current,  $E_b$  is plate-to-cathode voltage (hereafter called simply "plate voltage"), and  $E_c$  is the grid-to-cathode voltage (hereafter called simply "grid voltage"). This formula is based on a number of simplifying assumptions, probably the most important of which is that the cathode/grid/plate geometry is geometrically simple. It has been derived exactly for concentric cylinders and for infinite flat plates. If you look closely at a type 76 tube, you can see that it was designed with a cylindrical structure. Similarly a 300B was clearly designed with a planar structure. Both of these tubes are known for their high degree of linearity.

Based on this formula, I worked out the performance on the computer for a variety of operating conditions. I found that with two non-dimensional ratios I could summarize hundreds of computer analyses. Before introducing them, let me mention the operating resistance  $R_O$ , which is the ratio  $E_b/I_o$ , as described in Part 1. I call it a resistance because it has the dimensions of a resistor - in fact, it is the value of a resistor that would draw the same current as the tube if it were substituted. Then the first non-dimensional ratio I will use is  $R_O/r_p$ , where  $r_p$  is the tube's plate resistance. The second ratio is  $R_L/R_O$ , the ratio of load resistance to operating resistance. In part 1, I said that a load resistance equal to  $R_O$  was a good initial guess; now we'll examine some variations of

this and see the effect.

The ratio  $R_O/r_p$  should be at least 4 to give a reasonable operating box without risking grid current. Sometimes you are forced to use a lower value, such as when the plate resistance is very high, but the output power and voltage become severely restricted in this case. I evaluated operation for values of  $R_O/r_p$  from 2.5 to 10, which corresponds to a higher  $E_b$  than most tubes are rated for.

I varied the load ratio  $R_L/R_O$  from 0.25 to 1.0. It is not completely impractical to operate as low as 0.25 if  $R_O/r_p$  is small, although at higher values of  $R_O/r_p$  this will result in cutoff for a substantial portion of the cycle and therefore high distortion.

Shown below are contour plots of power (normalized to the plate dissipation PD) and second harmonic distortion at full output. As you can see, low  $R_O$  and high  $R_L$  produce the lowest distortion, but also the lowest power. The best tradeoff is with high  $R_L$  (for lower distortion) and high  $R_O$  (for more power output).

This study has led to a set of "rules of thumb" that approximately summarize these results, and work reasonably well for linear triodes (for nonlinearities, see Part 3.) These give a good starting point, but each tube and circuit is unique. I don't pretend these are the very best operating points, only that they are a pretty good starting point.

$$R_O/r_p = 5 \quad R_L/R_O = 0.7$$

actually, as long as  $R_O/r_p$  is greater than 4,  $R_L/R_O = (R_O/r_p - 1.5)/(R_O/r_p)$  is pretty good.

The minimum value of  $R_L/R_O$  to avoid cutoff is  $(R_O/r_p - 3)/(R_O/r_p)$

Incidentally, for a plate dissipation of PD watts, it's handy to know that  $E_b = \sqrt{R_O PD}$

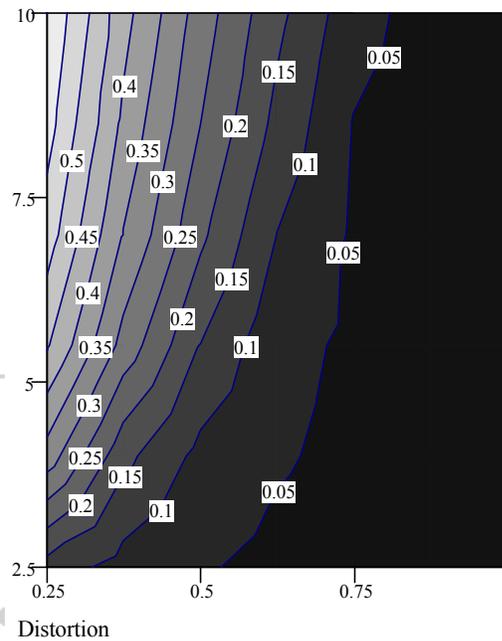
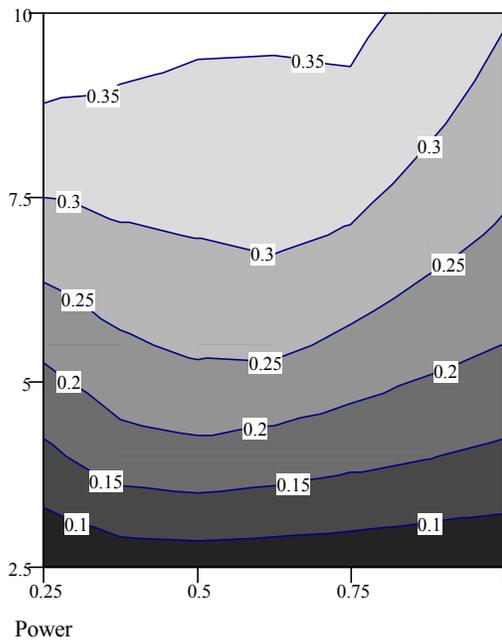
$$E_c = 0.7 E_b/m \quad \text{for } R_O/r_p = 5$$

actually,  $E_c = (E_b/m) (1 - 1.5/r_p/R_O)$  in general

$$\text{Hence } R_k = 3.5 r_p/m$$

$R_k$  is the cathode resistor

actually,  $R_k = (R_O - 1.5 r_p)/m$  in general. If  $R_L/R_O = (R_O/r_p - 1.5)/(R_O/r_p)$  as recommended above,



then  $R_k = R_L / m$ .

To complete the circuit for a single stage, we need the values for coupling and bypass capacitors, and for transformer or choke loaded stages, the load inductance. Assuming that the capacitors have a -3dB frequency of 5 Hz, we can estimate:

Bypass capacitor  $C_k = 65,000 / R_k$  microfarads,

coupling cap  $C_c = 30,000 / R_g$  microfarads ( $R_g$  is the grid resistor)

Now it is not so easy to make large inductors, so I generally assume that the minimum inductance value is that for which the impedance equals  $R_L$  at 40 Hz. This will give a small-signal frequency response down less than 1 dB at 40 Hz and less than 3 dB at 20 Hz, with a power bandwidth down 3 dB at 40 Hz. This value is:

Minimum choke or transformer primary inductance =  $R_L / 250$  henries

For a simple example, consider a 2A3 amplifier. The plate resistance  $r_p$  is 800 ohms according to the RCA manual. If we choose  $R_0 = 5$ , then  $E_b / I_b = 4000$ . For  $R_L / R_0 = 0.7$ , we get a load impedance of 2800 ohms. Plate voltage is  $\sqrt{15 R_0}$  at 15 watts, or 245 volts, and since  $P_D = 15$ ,  $I_b = 15 / 245 = 61$

mA. Grid voltage should be about -41 volts, if  $m$  is 4.2. The cathode resistor would be 667 ohms with a bypass of 97.5 microfarads. These values are pretty close to the RCA recommended operating point of 250 volts at 60 mA into a 2500 ohm load with 45 volts grid bias through a 750 ohm cathode resistor. With a maximum grid resistor of 500k ohms, a coupling cap of 0.06 microfarads would be big enough. Finally, a transformer of at least 10 henry inductance is needed for acceptable bass.

I have found these simple rules of thumb to be very useful when first developing a new design, or examining the possibilities for a particular transformer, tube, or power supply. Often there are reasons for varying these values (for instance, in my 300B amp the power supply and output transformer could not handle the estimated current of 80mA; I dropped it to 55mA which gave me more distortion but was still acceptable), but it's always nice to know where you are to start with. I hope you will find these rules as helpful as I have.