

FIG. 7-31

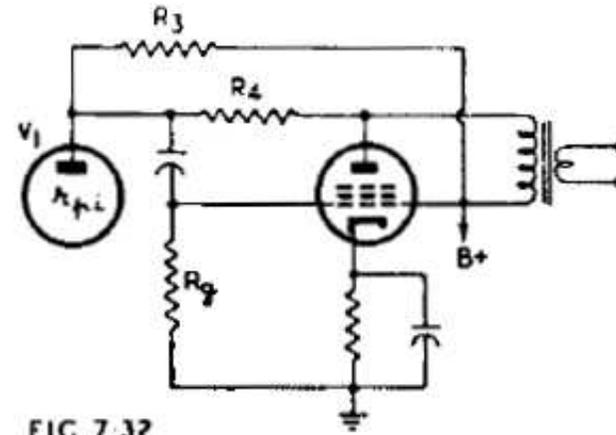


FIG. 7-32

Fig. 7.31. Voltage feedback applied in series with the load resistor. The reduction in effective resistance occurs in the load resistor itself.

Fig. 7.32. Electrically equivalent circuit to Fig. 7.31, using one less resistor.

Both these circuits (Fig. 7.31 and 7.32) have the effect of reducing the effective load into which  $V_1$  works. This has the merit of extending the response to higher audio frequencies. In Fig. 7.31 the effective value of  $R_L$  becomes

$$R_L' = R_L / (|\beta|A_2 + 1) \text{ where } |\beta| = R_1 / (R_1 + R_2)$$

and  $A_2$  is the numerical voltage gain of  $V_2$ . For example if  $|\beta| = 0.1$  and  $A_2 = 17$ , the effective load resistance changes from  $R_L$  without feedback to  $0.37 R_L$  with feedback. The load  $R_L'$  into which  $V_1$  works is, however, not constant because  $A_2$  varies due to distortion. This circuit is usually limited to values of  $|\beta|$  not greater than say 0.05 to 0.1 for typical applications.

A similar effect occurs with the equivalent circuit Fig. 7.32 in which the feedback causes the effective value of  $R_4$  to change to  $R_4 / (A_2 + 1)$ . In both circuits  $V_1$  is preferably a pentode, although a high-mu triode may be used with less effectiveness.