

- T₁ push-pull input, special channel mounting, no d.c. in primary; Freed 17290
- T₂ 4000 ohms plate to plate, 4-8-16-ohm secondary; Freed 15929
- T₃ 325-0-325 v at 50 ma; 5v at 2a; 6.3v at 2.5 a. Freed F-413
- X₁, X₂ 200 ma selenium rectifier

*Shown on diagram as 7500 ohms. This value should be adjusted to provide 36 volts across filament string.

The performance of any amplifier depends to a large degree upon the quality of the components used. At the time this amplifier was designed, it was desired to use high-quality transformers throughout, and to make the power section as compact as possible the input transformer had to be mounted underneath the chassis. This ruled against a cased type, and few manufacturers list high-quality transformers in open-frame mounting. The unit employed was designed to work between a single 12SJ7, triode connected, with no d.c. in the primary, and to obtain adequate driving voltage for the grids of the 6AS7G it was required that the step-up ratio should be fairly high. To get this performance and retain a wide frequency range, the transformer is wound in two sections, both placed on the center leg of a conventional E-I core. Measured frequency response of the transformer itself indicates a droop of 1 db at 30 cps and at 30,000 cps. The output transformer, also special, shows a droop of 1 db at 17 cps and at 120,000 cps when operated without feedback, and drooping 1 db at 15 cps and 62,000 cps when operated with feedback. Similar output transformers are available in the standard Freed line under number F-1951 with output impedances of 1.2 to 30 ohms, and under number F-1950 for impedances from 50 to 500 ohms.

The following table indicates transformers of high quality which are generally obtainable from jobber stocks and which should perform satisfactorily, since their characteristics are similar to those used in the original amplifier.

Construction Hints

There are a number of suggestions which may be of interest in the construction of these two units. Refer-

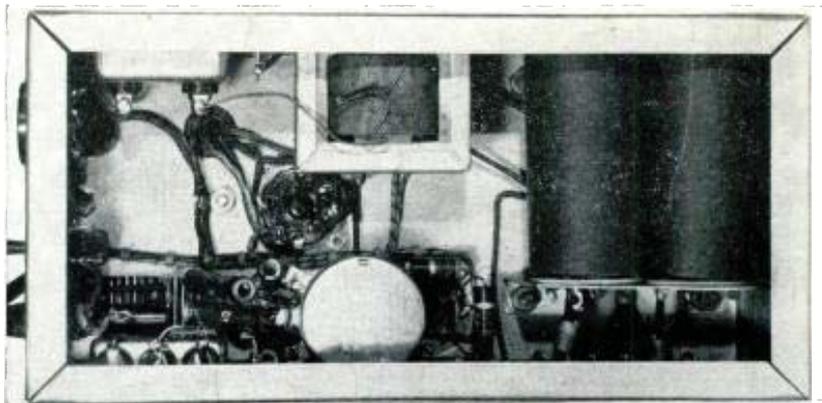


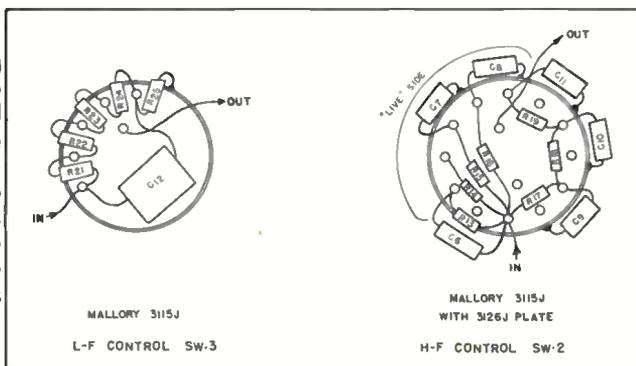
Fig. 2. Underside of power section chassis.

ring first to the power section, it will be noted that the two filter capacitors, C₃ and C₄, are mounted on a bracket under the output transformer. Therefore, they are necessarily installed after the wiring to the output transformer is completed. The balancing potentiometer, R₃, is also mounted on a bracket so that its shaft may be adjusted through a hole on the chassis between the two capacitors mounted on top. The selenium rectifiers are mounted on a 6-32 threaded rod which

The value for the resistor R₄ was shown as 7500 ohms. This gives somewhat too much current through the filament string, and it is found that 15,000 ohms is more suitable, since the voltage across the filaments should be 36 volts. R₇ has been added to reduce the peak current through the selenium rectifiers, and 5 ohms is a suitable value. This resistor is connected between SW₁ and C₃.

The push-pull input transformer is mounted directly below the 6AS7G

Fig. 3. Wiring diagram of two tone-control switches. Switch plate on H-F control is changed to furnish tie points on five-step frame. Only one contact arm is used.



passes through two strips of Bakelite attached to bent-up angles on the chassis. Two saw-cuts are made 3/4 in. apart and extending for two inches along the chassis. At the center of these two cuts, another cut is made between them. This frees two "flaps" which may be bent up to mount the Bakelite strips. The cover is bent up from perforated metal to prevent accidental contact with hands or tools.

socket, using leads as short as possible. This will normally require that the leads be connected before the transformer is bolted in place, and since the leads are likely to be of relatively light wire, care should be exercised in this operation. The two bathtub capacitors are mounted on opposite sides of the chassis, with tie-points installed adjacent to them. One is needed to make the connection to the plate end of the primary, and the other serves to hold R₇.

With some transformers it is probable that there will be a tendency to oscillate at some super-audible frequency. This may require some experimentation, but it is suggested that a small capacitor across each half of the primary of the output transformer, or possibly across the secondary of the input transformer, will suffice to eliminate this trouble. Probable values

TABLE I

	T ₁	T ₂	T ₃
Audio Development Co.	214H*	314C	515C
	215C*	315F	(large)
Chicago Transformer Div.	—	BO-6	PCC-70
Stancor	A-4750	A-3800	P-4078
Thordarson	T20A22	T22S70	T22R02
UTC	LS-21*	LS-57 ¹	R-54
	CG-132*	LS-55 ²	
		CG-16	

*Insufficient space under chassis to mount these models.

¹Voice coil secondary only. ²Voice coil and line secondary.

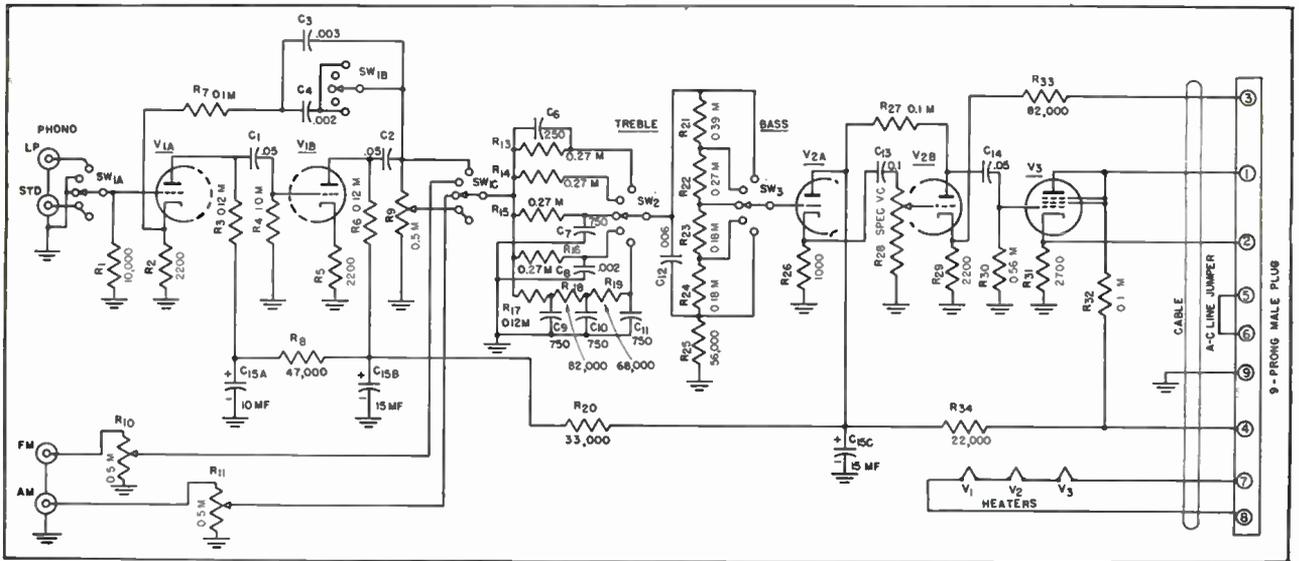


Fig. 4. Schematic of input section, with component values.

will be in the vicinity of .002 μ f. Figure 1 is a partial wiring diagram of parts employed in the power section, while Fig. 2 is a photograph of the underside of the completed amplifier chassis.

The preamplifier section shown in the photograph of Part 1 is somewhat smaller than the average constructor may wish to employ, but it was built in this manner to keep the space required to a minimum. The chassis was fabricated from a 2 x 7 x 11 aluminum chassis base, cutting it apart at the center. The sides of the chassis are then cut 1 1/4 in. from the open end, and folded in to provide a 3/8-in. angle. The top is folded down, resulting in a chassis approximately 3 1/2 x 7 x 2. The tube sockets and the electro-

lytic capacitor are mounted on this section, with the controls on the opposite side of the chassis. The input selector switch is mounted on one end, with a lever extending through the panel for its operation. If the chassis length were extended to eight or nine inches, the selector switch could then be mounted on the front in line with the other controls, and it is quite probable that it would be easier to install in a cabinet because of the difficulty in cutting a neat slot to pass the lever-type arm used to actuate the selector switch.

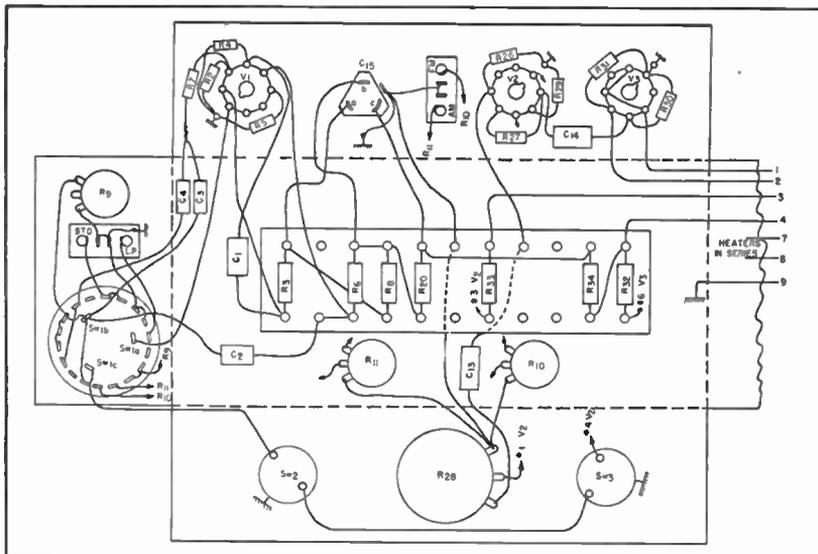
In the parts list several references were made to the text for further explanation. The volume control, R28, is the loudness control described in the February issue,¹ and consists of a

Centralab 1443 switch on which are mounted the resistors and capacitors necessary to obtain the desired compensation.

The high-frequency tone control switch, SW₂, needs a little further description. The series of switches selected for the tone controls consists of small units which are desirable in such a compact amplifier. However, the exact assembly of contacts is not obtainable, so the switch used was made by using the frame and mechanism from a 3115J switch with the contact plate from a 3126J switch. This gives a number of tie points for the resistors used for the cut-off circuit, as well as for the input connection. The capacitors in this circuit are all mounted directly on the switch, being soldered to the frame for ground connection. This is not usually considered the best practice, but it must be remembered that this section of the amplifier does not have any a-c circuits in it, and there is little chance of ground loops causing hum trouble. Suffice that the unit as constructed exhibits no troubles from this source. The exact arrangement of the tone controls is shown in Fig. 3. Similar methods were used for both, in that all parts are wired directly to the switch, but the low-frequency control is a standard 3115J switch without modification.

The overall schematic, Fig. 4, is essentially a repetition of the schematic published last month, with the removal of R₁₂ and C₅ as previously discussed. The wiring diagram, Fig. 5, indicates the arrangement of parts and the wiring between them, while

Fig. 5. Input section wiring diagram.



¹"Full Range Loudness Control," Winslow, AUDIO ENGINEERING, Feb. 1949.

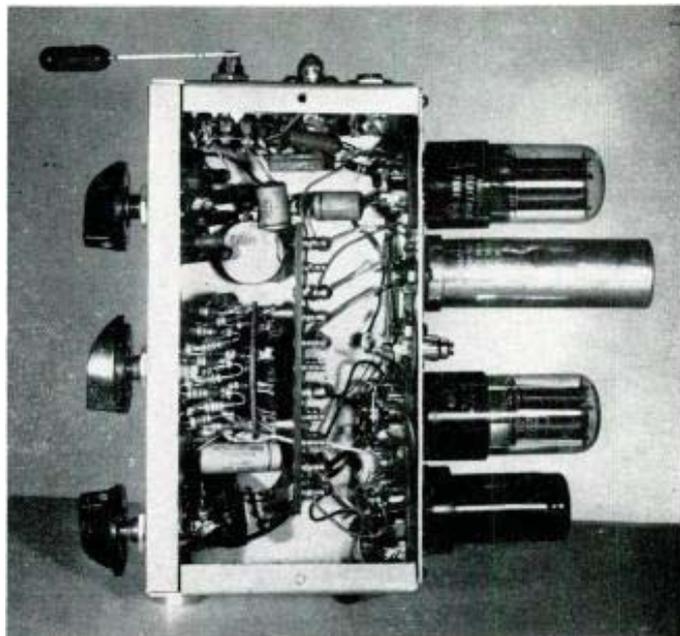
the photograph of Fig. 6 shows the method of mounting the resistor strip on the back of the volume control switch.

Unless the builder is reasonably well experienced in construction of small amplifier equipment, it might be desirable to increase the overall size of the input section. It is definitely possible to construct the unit in the size shown, but it must be admitted that it is extremely compact, and as the size is reduced the complexity of construction is increased. Of course, once the amplifier is completed there should be no need to get at it again, assuming that the constructor takes reasonable care in the selection of resistor and capacitor ratings to prevent the possibility of failure in use.

A more conventional construction of this entire amplifier would undoubtedly reduce the hum level still further, and if a larger power transformer were used—one which could supply the 0.9 amps of filament current required by three 6-volt tubes in the input section—the electrostatic field existing between heater and cathode of the present first 12SL7 would be reduced. If made in two units, however, it would be preferable to use a separate cable from the power section to the preamplifier to carry the heater current, although the signal from the preamplifier to the power section is of a relatively high level and it is possible that no trouble would be encountered from this source.

If additional gain is required, the cathode follower section of V_2 can be changed to a conventional amplifier, thus giving approximately 32 db more

Fig. 6. Interior of input section, showing the mounting of resistor strip on rear of compensated volume control.



gain than with the present arrangement. For the uses for which this amplifier was designed, however, this should not be necessary. Another possibility is that a 6SN7 could be substituted for the 6SL7 used as V_2 , (if a filament transformer were being used, together with 6-volt tubes) again using the amplifier connection rather than the cathode follower, and the increased gain would be of the order of 10 db. This suggestion would only apply if the filaments were arranged to be supplied from a transformer winding, since the 12SN7 will not operate in a series string with the 12SL7 and the 12SJ7, inasmuch as

the 12SN7 draws a filament current of 0.3 amps. These are design modifications, and some ingenuity on the part of the constructor will be necessary to arrive at the exact desired result. It is felt, however, that the amplifier as described performs satisfactorily, and that no changes are necessary for the purpose for which it was designed. The amplifier was designed for one application—that of modernizing an existing installation, or for providing a control arrangement which could be adapted to cramped quarters with the greatest of ease. This requirement is fulfilled adequately by the arrangement shown.

Measuring Procedures for Magnetic Recording

ABOUT three years ago the Radio Manufacturers Association organized a subcommittee of the Committee on Phonograph Combinations and Home Recording to suggest standards for magnetic recording equipment. A series of sub-subcommittees were formed shortly thereafter, one of which was commissioned to work on "magnetic recording terminology" and to propose measuring procedures for magnetic recording. This sub-subcommittee has now released recommendations for measuring procedures for magnetic recording.

While it fully recognized that this material will be subject to modification with additional knowledge becoming available, it is felt that it presents a valuable basis for comparing the performance of various types of magnetic home recording equipment. To give this tentative proposal as wide a circulation as possible, the RMA Subcommittee on Magnetic Recording has approved its publication at this time.

Particular attention is called to the section on Noise which is subdivided into System Noise and Medium Noise. This subdivision has been suggested since in most cases the inherent noise generated by a completely neutralized medium is lower than the noise which might be expected in a typical magnetic recorder. It should be kept in mind, however, that noise measurements made, even on a properly neutralized medium, can produce indefinite results. To illustrate this point, a slightly magnetized reproducing head can greatly affect the noise generated by the magnetic recording medium and ambiguous results might be obtained.

For the proper evaluation of a medium, not only the ground noise of the medium as such is important but also the modulation noise (noise-behind-the-signal). No recommendations are presently available for an acceptable procedure for determining the noise-behind-the-signal. There can, however, be no question that there is a gap in the measuring procedures which eventually has to be bridged.

Another problem with which the investigator of magnetic recording equipment is confronted is the determination of amplitude variations which are experienced in reproduction when steady tone signals have previously been recorded. The performance of a magnetic recorder depends greatly upon the magnitude of such amplitude variations. Measuring procedures should eventually be provided to evaluate this deficiency of mediums and of complete magnetic recording systems.

Measuring Procedures for Magnetic Recording

RMA Sub-committee on Nomenclature and Measurements
RMA Subcommittee on
Magnetic Recorders R7.4

1. FREQUENCY RESPONSE OF UNEQUALIZED SYSTEM

The frequency response of a magnetic recording system depends upon the medi-

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