

A Simple Phono Preamp Using A Pair Of 6DJ8/ECC88 Tubes

http://www.geocities.com/Tokyo/Temple/9151/rjmaudio/diy_pho3.html

Here is a phono pre-amplifier having a gain of about 40dB, passive RIAA equalization, two tubes, and simple circuitry. The 6DJ8/ECC88 dual triode tube was chosen for its relatively low output impedance, reasonably high gain, and ready availability. The operating points are set conservatively to ensure long life and high reliability. I wanted to design an easy to build, easy to use, easy to power, and easy to listen to device.

The Amplifier Circuit

Circuit walk through:

The input signal from the cartridge is fed into the grid of V1, through a 500 ohm grid stopper resistor R2 to prevent oscillations. V1 multiplies the signal by about 30 times. It is then equalized to the RIAA standard curve by a frequency-variable voltage divider which drops the signal voltage by a factor of 10 on average. This is essentially the same voltage divider network found in the previous project, the op-amp phono stage. The output is capacitively coupled through C3 to the next gain stage, with another grid stopper resistor R8. R8 is not optional; the amplifier will oscillate otherwise. V2 multiplies the signal by another factor of 30. The output from the plate of V2 is coupled through C4 to block the DC voltage before being routed to the output RCA jack. Total gain about $30 / 10 \times 30 = 90$.

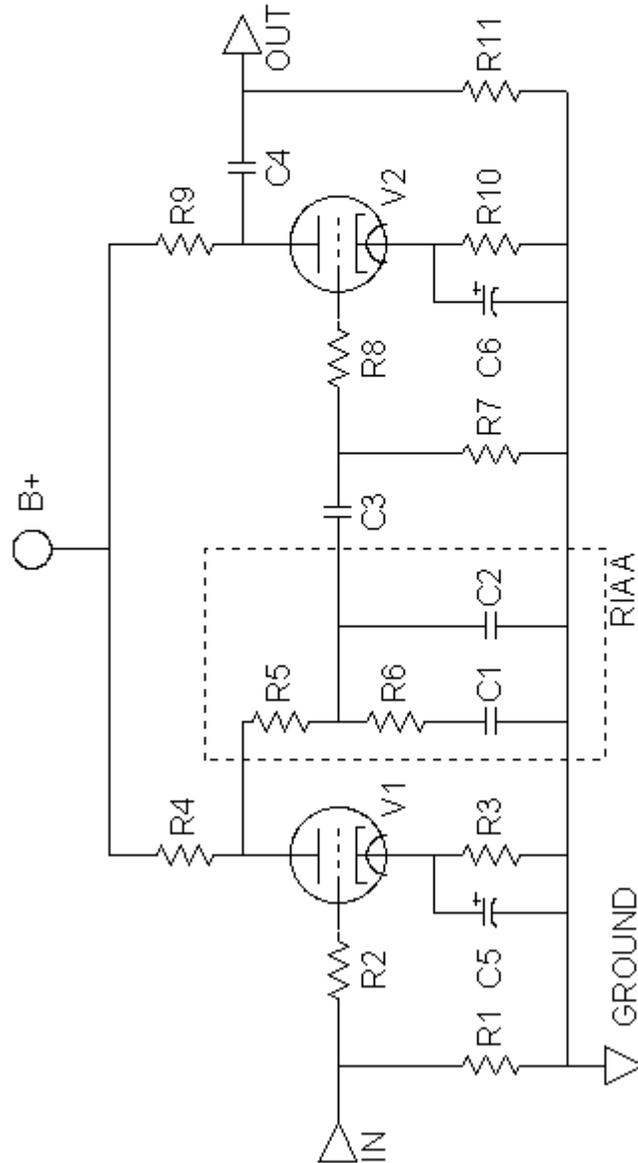
The RIAA equalization network comprising R5,R6,C1,C2 is set taking the output impedance of V1 into consideration as well as the grid resistor R7. C3, C8, R8 and the miller effect in V2 may be safely ignored. The MathCAD model shows a linear response +/- 0.1 dB over the audio band, with the normal roll-off at both extremes caused by other circuit considerations. This was confirmed on the test bench, the measured deviation being within +/- 0.2 dB 20-20kHz.

As always there is some benefit to using high quality components, especially the cathode bypass capacitors C5 and C6. Audio grade electrolytics here, and polypropylene, polystyrene or audio-specific coupling caps for the rest of the capacitors. As for tubes I have used the Amperex Bugle Boy 6DJ8s and would recommend them. They seem to be a smooth sounding, low noise tube. Mullard brand 6DJ8's are very similar.

Recent Revisions : I upgraded to Holco resistors and Black Gates for C5 and C6. C3 was a 0.1 uF Multicap, while C4 was a 1.2 uF Solen. C5 and C6 may be reduced from 220 uF to 50 or 100 uF without any noticeable loss of bass response. The B+ voltage can be anything from 180V to 280V. All other things being equal, a lower B+ gives a warmer, richer sound at the expense of speed and detail. This is probably caused by the expected increase in bass response and second harmonic distortion, respectively. I run mine at 190V.

Design Note : Bass is controlled by R5 in series with the output impedance of V1. The larger these values, the greater the bass in the 50-100 Hz region. If the operating point of V1 is changed, then the output impedance will also change, and R5 may have to be adjusted to compensate.

2x 6DJ8 MM phono stage (gain ~38dB)



B+ : 250 V

V1,V2 : 1/2 ECC88 6DJ8

C1 : 0.03uF/400V 1% RIAA

C2 : 0.01uF/400V 1% RIAA

C3 : 0.1uF/400V coupling

C4 : 1.0uF/400V coupling

C5,C6 : 220uF/10V bypass

R1 : 47k (as per cartridge spec.)

R2,R8 : 500R 1/4W grid stopper

R3,R10 : 500R 1/4W cathode bias

R4,R9 : 30k 2W plate resistor

R5 : 83k 1/4W 1% RIAA

R6 : 10.5k 1/4W 1% RIAA

R7 : 470k 1/4W grid resistor

R11 : 470k 1/4W load resistor

note 1 : RIAA values adjusted for Rp of V1, and R7.

note 2 : Bass response is limited by C4, and should be adjusted for the input impedance of the

stage it will drive. 1.0uF results in -3dB at 20Hz into 100k.

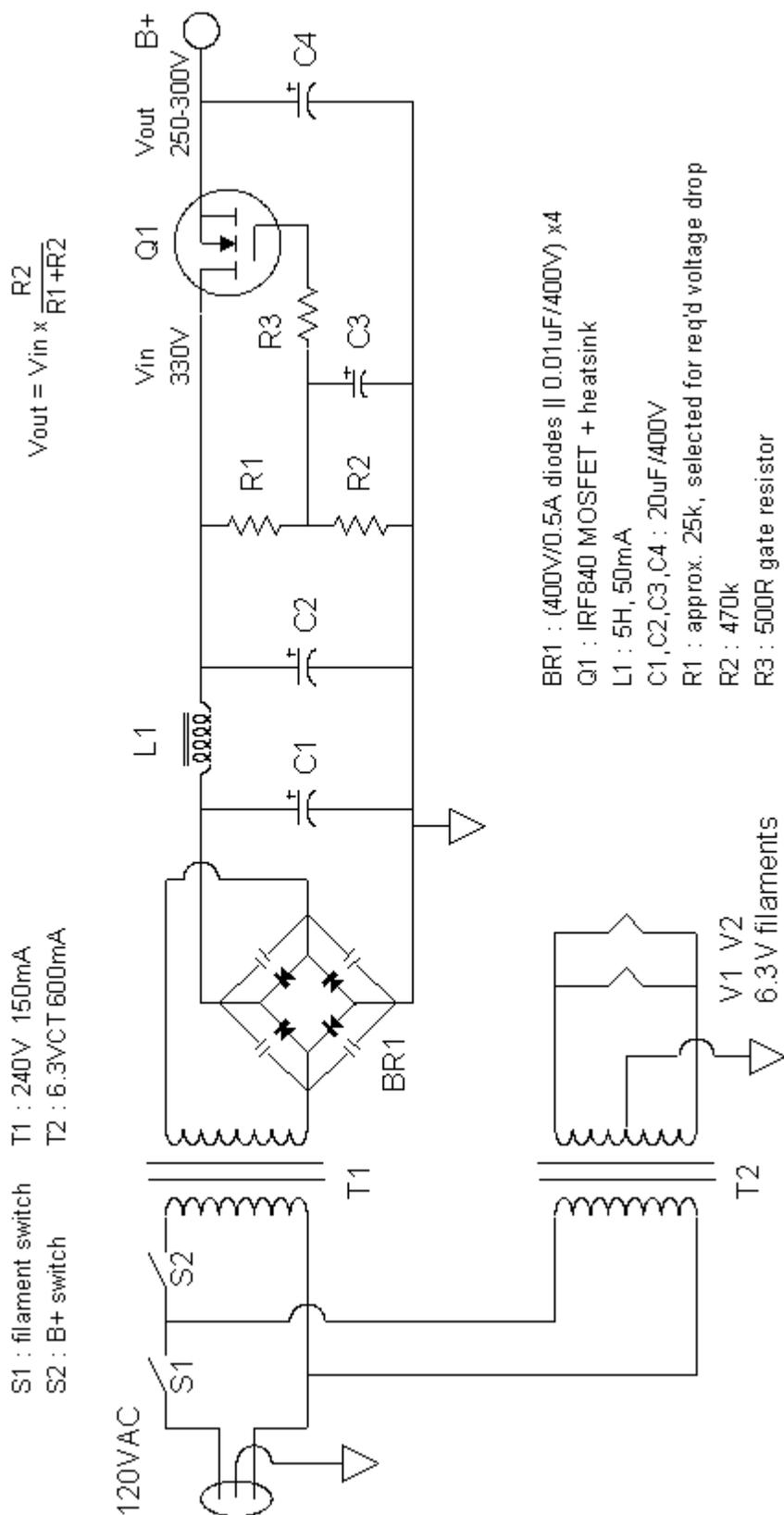
note 3 : Tubes operate at 100V, 5mA, with a 2.5V bias, dissipating 0.5W per section.

note 4 : C1 is made of 3x 0.01uF/400V capacitors in parallel.

Construction Note : I set this up with an external power supply, with only 16uF of Solen polypropylene B+ filter capacitance within the amplifier itself. The wiring was a mostly point-to-point, but the RIAA section and plate resistors were mounted on a single piece of perf-board. The only warning concerns the 30kohm plate resistors R3,R10. They dissipate just under 1W each, which is enough to get a 3W wire-wound resistor too hot to touch. Allow for some air circulation/heatsinking if possible.

I'm particularly proud of this simple MOSFET regulated power supply. Nothing fancy, it just removes the ripple from the B+ with the minimum of fuss and bother. The principle advantage, besides a ripple of under a millivolt, is the trivial amount of capacitance needed to get there. An all polypropylene or oil capacitor power supply is quite practical, as is an ultra-compact one if electrolytics are used.

MOSFET Regulated 300V~50mA Power Supply for a Tube Phono Amplifier



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N.B. C1 and C2 can be reduced to 8 uF, C3 can be lower as well, set according to the method outlined below. C4 can be larger, but the total output capacitance (including whatever is included on the B+ next to the preamp circuit, should not exceed 50 uF.

The MOSFET should be rated to a voltage greater than 1.4 times the transformer output, but can otherwise be substituted at will. Anything in the IRF 7xx and 8xx product families will be suitable. Buy at least two, as it is fairly easy to fry them when your project is in the prototype stage. Once connected properly they are very reliable.

The choke is needed to convert the ripple from a sawtooth wave typical of a capacitor input filter to a smoother sinusoidal waveform which is easier for the MOSFET to erase. 5-20 H is needed. The erasing part happens because the ripple causes the gate-source voltage of the MOSFET to change, and the gain/transconductance of the MOSFET is large enough that it compensates almost perfectly.

The gate-source voltage is only a couple of volts, so the voltage at the junction of R1 and R2 is essentially the same as the source/output. R1 is adjusted to get whatever voltage is required. The greater the drain-source voltage, the better the regulator copes with large ripple voltages and widely varying current loads, but the power dissipated by the MOSFET will be greater, requiring better heatsinking. Since the line ripple voltage and the current load variation are both very small in line audio circuits, a 25 to 50 volt drop is more than enough. The power dissipated by the MOSFET is *voltage drop x the current draw* of the load circuit. It is about 4W in the circuit shown, but only 1.5W when driving just the phono pre-amp, which draws 20mA.

This isn't an IC regulator like an LM7812. There is no absolute regulation, as there is no voltage reference. Neither is there any short circuit or thermal protection. It is better thought of as an unregulated power supply with really good filtering and very low output impedance than a true regulated supply.

For all its simplicity, there are a couple of useful side effects. When switched on, there is an initial turn on delay before the output voltage is at maximum. The time constant is equal to $R1 \times C3$. This is also the low frequency cutoff below which the regulator does not function, so should be kept above 50ms (10Hz or less).

I consider the absence of an inherently noisy voltage reference (zener or gas discharge tube) more or a plus than a minus, as I do the absence of feedback. The filtering is so good that the B+ can be applied directly to the plate of the input tube without needing a dropping resistor and extra filter capacitor, the result is fewer parts and a lower power supply impedance.

The regulator is like an inverse amplifier, it amplifies the power supply to compensate for load current changes as the music signal is amplified by the circuit. The lower the PSRR - *power supply rejection ratio* - of the amplifier, the more you hear what is going on in the power supply. Unbalanced, single-ended single-supply tube circuits don't have good PSRR, hence their sensitivity to regulation.

The supply is scaleable to larger voltages and currents, and it is easy to have separate regulation sections for each channel or even each tube. And yes, you could use tubes in the power supply too, and it might be even better. The solid state diodes could be swapped for a 6X4 or 6CA4 rectifier tube, but you'd need a center-tapped 650V power transformer. The MOSFET could be replaced by a power triode, but to get the current capacity you might have to use one for each channel, and the gain might be too low, requiring a voltage reference and comparator triode amplifier. In short, do-able, but not quite as elegant. For a great discussion of tube voltage regulators, see the TubeCAD Website.

(Another) Power Supply

This is the power supply I use. 6CA4 tube rectifier, and an LCLC filter instead of the MOSFET. Less trouble, lower ripple, and (slightly) better sound. The chokes are not expensive, since the current is so low. The value of L2 is not critical, 5H may be better. The amount, type of C1 and C2 does affect the sound. Oil caps worked best for me, Solen

polypropylene a close second. More uF's may not always sound better. The output is about 250V. C3, C4, L3, L4 are just to try and remove high frequency hash from the AC line, and can be considered optional.

Phono Preamplifier LCLC Power Supply

