



(12) **UK Patent** (19) **GB** (11) **2 405 275** (13) **B**

(45) Date of publication: **10.05.2006**

(54) Title of the invention: **Amplifiers**

(51) INT CL: **H03F 1/02** (2006.01) **H03F 3/30** (2006.01)

(21) Application No: **0417832.3**

(22) Date of Filing: **11.08.2004**

(30) Priority Data:
(31) **0319706** (32) **22.08.2003** (33) **GB**

(43) Date A Publication: **23.02.2005**

(52) UK CL (Edition X):
H3W WUE
H3T T2RX T2T3B T2T3F T3J T3N T4D T6P1

(56) Documents Cited:
JP 560103508 A **JP 050022048 A**
JP 2004260395 A

(58) Field of Search:
As for published application 2405275 A viz:
UK CL (Edition W) **H3W**
INT CL⁷ **H03F**
Other:
updated as appropriate

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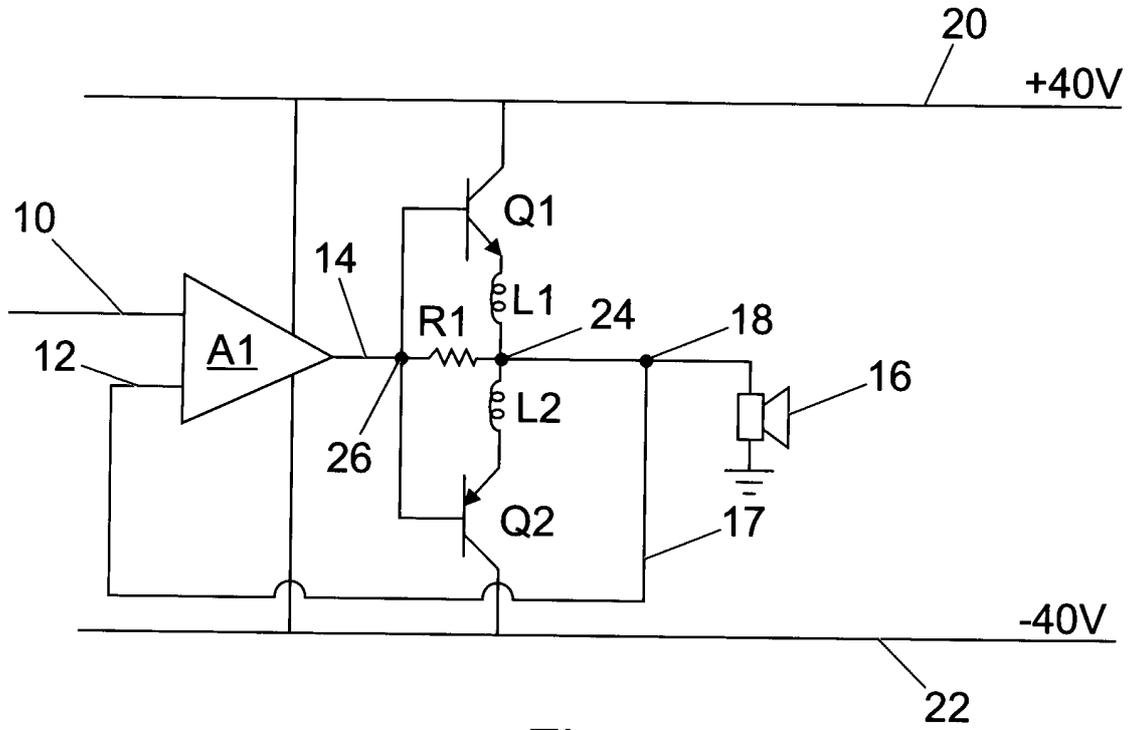


Fig. 1

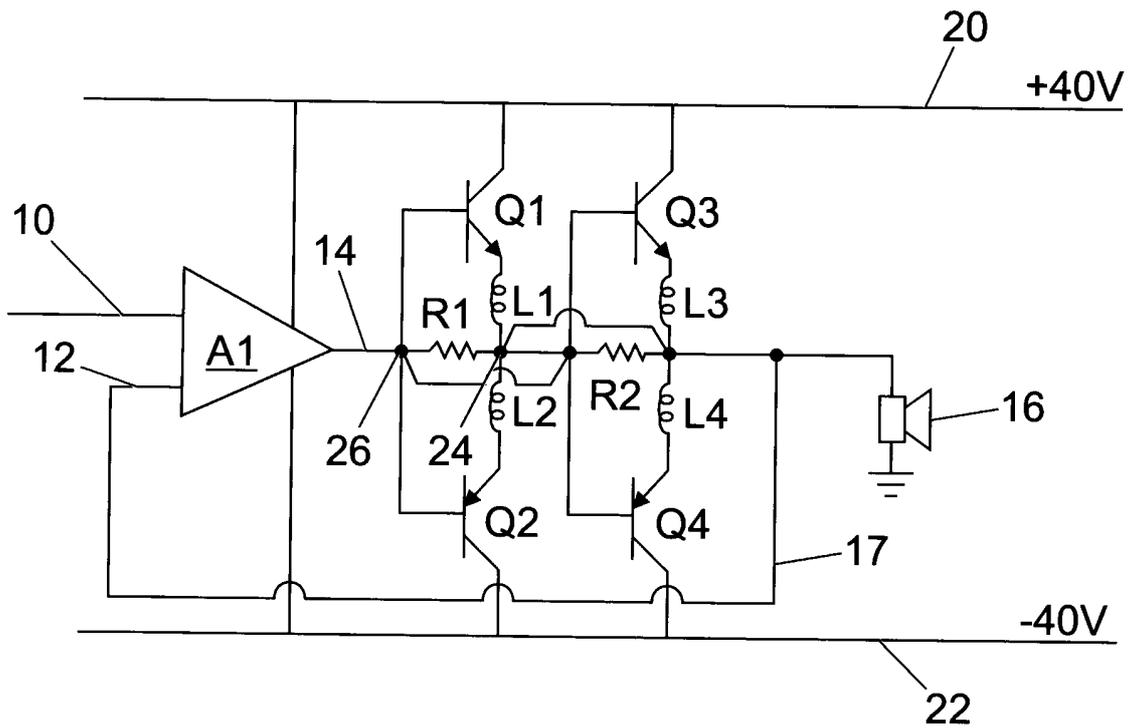


Fig. 2

1 Amplifiers

2

3 The present invention relates to amplifiers,
4 particularly but not exclusively linear audio power
5 amplifiers.

6

7 Most 'high end' audio power amplifiers are built
8 using many discrete components: transistors, diodes,
9 resistors, capacitors etc. An alternative approach,
10 used generally in lower performance, lower power
11 applications, uses single silicon chip 'monolithic'
12 power amplifiers where essentially the entire
13 amplifier circuit is integrated on to one or a few
14 chips and packaged in one device. A minimal number
15 of external parts are required to complete the
16 application. Some high performance monolithic
17 amplifier solutions can be adapted for 'high-end'
18 use.

19

20 The advantage of monolithic amplifier solutions is
21 that it is possible to integrate much more complex
22 circuitry than could be practically built with

1 discrete components, giving the potential for very
2 high performance. Their disadvantage is that their
3 power handling is limited. This invention concerns a
4 method of combining the advantages of monolithic
5 chips and discrete transistors to create compact,
6 reliable high performance audio amplifiers, very
7 simply.

8
9 It is known to add a number of discrete 'booster'
10 transistors on to the output of a monolithic
11 amplifier. The monolithic generates all the output
12 power up to a very safe and defined limit, then the
13 booster transistors switch on to provide virtually
14 unlimited further power. The potential problem with
15 this type of arrangement is the discontinuity at the
16 instant when the boosters switch on and off. The
17 present invention provides a simple and effective
18 solution to this problem, requiring only the
19 addition of small inductors.

20
21 In accordance with a first aspect of the present
22 invention, there is provided an amplifier
23 comprising:

24 a primary power amplifier comprising at least
25 one integrated circuit and having a signal input and
26 an output, the output being connected to a first
27 output node; and

28 a secondary amplifier formed from discrete
29 components and connected between the output of the
30 primary amplifier and said first output node, said
31 secondary amplifier being operable to boost the
32 output from the primary amplifier in response to the

1 output current from the primary amplifier reaching a
2 predetermined threshold value; wherein

3 said secondary amplifier includes at least one
4 inductance for extending a switching off period of
5 said secondary amplifier.

6

7 Preferably, said secondary amplifier comprises at
8 least a first amplifier stage including:

9 first and second complementary transistors,
10 first and second inductances and a resistance;

11 said first transistor having a power supply
12 terminal connected to a positive power supply, an
13 output terminal connected via said first inductance
14 to a second output node located between said primary
15 amplifier output and said first output node, and a
16 control terminal connected to a third output node
17 located between said primary amplifier output and
18 said second output node;

19 said second transistor having a power supply
20 terminal connected to a negative power supply, an
21 output terminal connected via said second inductance
22 to said second output node, and a control terminal
23 connected to said third output node; and

24 said resistance being connected between said
25 second and third output nodes for setting said
26 threshold value for switching said first and second
27 transistors.

28

29 Preferably, a feedback loop connects said first
30 output node to a feedback input of the primary power
31 amplifier.

32

1

2 In alternative embodiments, the secondary amplifier
3 may include a plurality of similar amplifier stages
4 cascaded within said feedback loop.

5

6 Preferably, said primary power amplifier is a
7 monolithic amplifier solution comprising at least
8 one integrated circuit.

9

10 Preferably, transistors of said secondary amplifier
11 comprise bipolar transistors.

12

13 Embodiments of the present invention will now be
14 described, by way of example only, with reference to
15 the accompanying drawings in which:

16 Fig. 1 is a circuit diagram illustrating a preferred
17 embodiment of the present invention; and

18 Fig. 2 is a circuit diagram exemplifying alternative
19 embodiments of the present invention.

20

21 Referring now to the drawings, amplifier A1
22 represents a monolithic linear audio amplifier
23 solution, which may comprise one or more integrated
24 circuits. Solutions of this type are well known in
25 the art and will not be described further herein.

26 Amplifier A1 has a first signal input 10 for
27 receiving an input signal, a second feedback input
28 12 and an output 14 connected, in use, to a
29 loudspeaker 16 or other output transducer or the
30 like. A feedback path 17 connects the feedback
31 input 12 to a first node 18 between the output 14
32 and the loudspeaker 16. Positive and negative DC

1 power supply rails 20 and 22 are also connected to
2 the amplifier A1 in a conventional manner.

3
4 A booster circuit, formed from discrete components
5 for boosting the output current from amplifier A1
6 includes a complementary pair of first and second
7 transistors Q1 and Q2 and resistance R1. In
8 preferred embodiments the transistors Q1 and Q2 are
9 bipolar transistors (one n-p-n type and one p-n-p
10 type). The collectors (power supply terminals) of
11 the transistors Q1 and Q2 are connected to the
12 positive and negative power rails 20 and 22
13 respectively. The emitters (output terminals) of
14 the transistors Q1 and Q2 are connected to a second
15 node 24 between the amplifier output 14 and the
16 first node 18 (i.e. inside the feedback path 17).
17 The bases (control terminals) of the transistors Q1
18 and Q2 are connected to a third node 26 between the
19 amplifier output 14 and the second node 24. The
20 resistance R1 is connected in series between the
21 second and third nodes 24 and 26.

22
23 In operation of the circuit as described thus far,
24 transistors Q1 and Q2 are both switched off as long
25 as the output current from the amplifier A1 is below
26 a threshold determined by the value of resistance
27 R1. When the threshold current is reached, the
28 complementary transistors Q1 and Q2 are switched on
29 alternately on positive and negative parts
30 respectively of the current cycle, thereby providing
31 additional amplification of the output signal from
32 the amplifier A1.

1

2 A problem with the arrangement as described above
3 arises because the transistors Q1 and Q2 do not
4 switch on and off instantaneously, causing
5 discontinuities in the current/time characteristic
6 of the final output to the loudspeaker 16. This is
7 easily remedied for switching on, by setting the
8 threshold so that the transistors switch on "early".
9 However, there remains a problem with discontinuity
10 of the power output at switch off.

11

12 Biasing the transistors Q1 and Q2, so as to reduce
13 their switching period, would mitigate this problem,
14 but the complexity of suitable biasing circuitry
15 would defeat the purpose of using a monolithic
16 amplifier solution.

17

18 In accordance with the present invention, the
19 problem is solved by the use of inductances L1 and
20 L2, one of which is connected between the emitter of
21 each of the respective transistors Q1 and Q2 and the
22 second node 24.

23

24 The inductances L1 and L2 have the effect of slowing
25 down the switching off of the transistors Q1 and Q2,
26 thereby smoothing any discontinuity that might occur
27 at the switching of the transistors. At switch off,
28 as the output current of Q1 or Q2 falls below the
29 threshold, the emitter voltage briefly (i.e. for a
30 period on the order of microseconds) drops below the
31 base voltage so that the decaying inductor current
32 circulates from the emitter to the base of the

1 transistor, keeping the transistor turned on for a
2 period (again on the order of microseconds,
3 determined by the time constant of the inductive
4 circuit), sufficient to smooth any switching
5 discontinuity.

6
7 In a typical application, the transistors Q1 and Q2
8 will be switched off until the output from the
9 monolithic amplifier A1 reaches a threshold of about
10 5A, and will then switch on to boost the output as
11 required. The value of resistor R1, which
12 determines the switching threshold, might typically
13 be about 100 m Ω and the inductance of L1 and L2 of
14 the order of several μ H, in order to provide a time
15 constant of the order of microseconds. The values
16 of L1 and L2 are not critical, being determined by
17 the required switching speed. If they are too
18 large, transistor switch-on will be too slow; if too
19 small, the switch-off delay effect will be
20 insufficient.

21
22 Bipolar transistors are preferred, but MOSFETs could
23 be used instead.

24
25 Fig. 1 shows the amplifier having a single booster
26 stage, but it will be understood that multiple
27 booster stages can be provided by cascading multiple
28 booster circuits similar to that of Fig. 1 within
29 the feedback loop 17. Fig. 2 shows a circuit with
30 two cascaded booster stages.

31

1 The invention enables the advantages of monolithic
2 amplifier solutions to be exploited while allowing
3 the output of the monolithic amplifier to be boosted
4 to any required level without distortion in a simple
5 and cost-effective manner.

6

7 Improvements and modifications may be incorporated
8 without departing from the scope of the invention.

1 Claims

2

3 1. An amplifier comprising:

4 a primary power amplifier comprising at least
5 one integrated circuit and having a signal input and
6 an output, the output being connected to a first
7 output node; and8 a secondary amplifier formed from discrete
9 components and connected between the output of the
10 primary amplifier and said first output node, said
11 secondary amplifier being operable to boost the
12 output from the primary amplifier in response to the
13 output current from the primary amplifier reaching a
14 predetermined threshold value; wherein15 said secondary amplifier includes at least one
16 inductance for extending a switching off period of
17 said secondary amplifier.

18

19 2. An amplifier according to claim 1, wherein said
20 secondary amplifier comprises at least a first
21 amplifier stage including:22 first and second complementary transistors,
23 first and second inductances and a resistance;24 said first transistor having a power supply
25 terminal connected to a positive power supply, an
26 output terminal connected via said first inductance
27 to a second output node located between said primary
28 amplifier output and said first output node, and a
29 control terminal connected to a third output node
30 located between said primary amplifier output and
31 said second output node;

1 said second transistor having a power supply
2 terminal connected to a negative power supply, an
3 output terminal connected via said second inductance
4 to said second output node, and a control terminal
5 connected to said third output node; and

6 said resistance being connected between said
7 second and third output nodes for setting said
8 threshold value for switching said first and second
9 transistors.

10

11 3. An amplifier according to claim 1 or claim 2,
12 wherein a feedback loop connects said first output
13 node to a feedback input of the primary power
14 amplifier.

15

16 4. An amplifier according to claim 3, wherein the
17 secondary amplifier includes a plurality of similar
18 amplifier stages cascaded within said feedback loop.

19

20 5. An amplifier according to any preceding claim,
21 wherein said primary power amplifier is a monolithic
22 amplifier solution comprising at least one
23 integrated circuit.

24

25 6. An amplifier according to any preceding claim,
26 wherein transistors of said secondary amplifier
27 comprise bipolar transistors.

28

29 7. An amplifier substantially as hereinbefore
30 described with reference to the accompanying
31 drawings.