

# Quickly discharge power-supply capacitors

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**A** PERENNIAL CHALLENGE in power-supply design is the safe

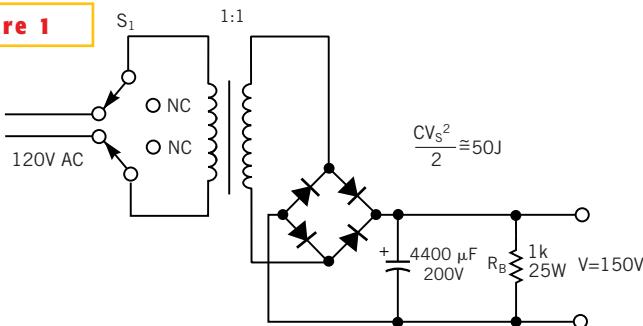
and speedy discharge, or “dump,” at turn-off of the large amount of energy stored in the postrectification filter capacitors. This energy,  $CV^2/2$ , can usually reach tens of joules. If you let the capacitors self-discharge, dangerous voltages can persist on unloaded electrolytic filter capacitors for hours or even days. These charged capacitors can pose a significant hazard to service personnel or even to the equipment itself.

The standard and obvious solution to this problem is the traditional “bleeder” resistor,  $R_B$  (Figure 1). The trouble with the  $R_B$  fix is that power continuously and wastefully “bleeds” through  $R_B$ , not only when it’s desirable during a capacitor dump, but also constantly when the power supply is on. The resulting energy hemorrhage is sometimes far from negligible.

Figure 1 offers an illustration of the problem, taken from the power supply of a

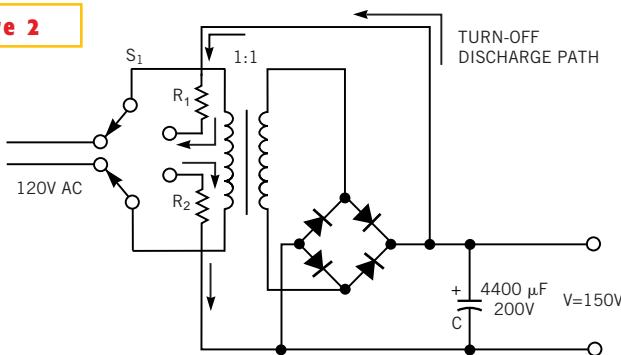
pulse generator. The  $CV^2/2$  energy stored at the nominal 150V operating voltage is  $150^2 \times 4400 \mu\text{F}/2$ , or approximately 50J. Suppose you choose the  $R_B$  fix for this supply and opt to achieve 90% discharge of the 4400- $\mu\text{F}$  capacitor within 10 sec after turning off the supply. You then have to select  $R_B$  to provide a constant RC time no longer than  $10/\ln(10)$ , or 4.3 sec.  $R_B$ , therefore, equals 4.3 sec/4400  $\mu\text{F}$ , or approximately 1 k $\Omega$ . The resulting continuous power dissipated in  $R_B$  is  $150^2/1 \text{ k}\Omega$ , or approximately 23W. This figure represents an undesirable power-dissipation

Figure 1



A bleeder resistor ensures safety but wastes much power.

Figure 2



Otherwise unused switch contacts can dump energy while not wasting power.

penalty in a low-duty-cycle pulse-generator application. This waste dominates all energy consumption and heat production in what is otherwise a low-average-power circuit. This scenario is an unavoidable drawback of bleeder resistors. Whenever you apply the 10%-in-10-sec safety criterion, the downside is the inevitable dissipation of almost half the  $CV^2/2$  energy during each second the circuit is under power.

Figure 2 shows a much more selective and thrifty fix for the energy-dump problem. The otherwise-unused off-throw

contacts of the DPDT on/off power switch create a filter-capacitor-discharge path that exists only when you need it: when the supply is turned off. When the switch moves to the off position, it establishes a discharge path through resistors  $R_1$  and  $R_2$  and the power transformer’s primary winding. The result is an almost arbitrarily rapid dump of the stored energy, while the circuit suffers zero power-on energy waste. Use the following four criteria to optimally select  $R_1$ ,  $R_2$ , and  $S_1$ :

- The peak discharge current,  $V/(R_1 + R_2)$ , should not exceed  $S_1$ ’s contact rating.
- The pulse-handling capability of  $R_1$  and  $R_2$  should be adequate to handle the  $CV^2/2$  thermal impulse. A 3W rating for  $R_1$  and  $R_2$  is adequate for this 50J example.
- The discharge time constant,  $(R_1 + R_2)C$ , should be short enough to ensure quick disposal of the stored energy.
- $S_1$  must have a break-before-make architecture that ensures breaking both connections to the ac mains before making either discharge connection, and vice versa. Otherwise, a hazardous ground-fault condition may occur at on/off transitions.

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